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Сору #

OPTICAL TECHNOLOGY DIVISION

PROJECT MEMORANDUM

PM-1519-X

19 AUGUST 1974

SENSOR SYSTEM POST FLIGHT REPORT

SV-8 (S/N 011)

Prepared by:

Flight Operations and Evaluation Section

Reviewed by:

F.L. HARRIGAN, JR. Manager Flight Operations and Evaluation

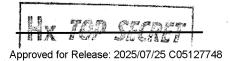
Approved by:

W.C. COTTRELL, Manager Field Operations Department

	PROJECT MEMORANDUM NUMBER:	PM-1519-X
	PREPARED BY;	Flight Operations & Evaluation
	DATE:	19 AUGUST 1974
•	SUBJECT:	Sensor System Post Flight Report SV-8 (S/N 011)
	DISTRIBUTION:	SP-7 (2) WCFO (2) SSC/DCO R. Jones W. Keeney J. Garrish P. Petty C. Karatzas L. Weeks
	ABSTRACT:	This report outlines the flight history for the SV-8 (S/N OII) Sensor System.
	DESCRIPTORS:	Flight Report, S/N 011 Flight Operations, S/N 011

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MISSION 1208

SENSOR SYSTEM OPERATION

POST FLIGHT REPORT

1.0 INTRODUCTION

1.1 Mission Objective

The primary objective of the Hexagon Mission is to provide high resolution photography. The intent of the eighth flight was to demonstrate functional operation of the primary satellite vehicle 93 day capability. This objective was surpassed with an active mission life of J05 days.

1.2 <u>Mission Description</u>

The Hexagon Mission 1208 satellite vehicle was launched from VAFB, SLC-4E, at 1320PST 10 April 1974 using a Titan 3p booster vehicle. The first recovery vehicle was successfully retrieved from the water and the remaining three recovery vehicles were successfully air retrieved within predicted impact dispersions. Recoveries were Day 14, 42, 69 and 105 respectively.

During testing at the launch base, a small leak was detected in the fwd camera pneumatics. The leak was determined to be between the high pressure isolation valve (HPIV) and the regulator. To prevent any loss of nitrogen gas during the mission it was decided to operate with the HPIV-A closed. The count down and launch phase were accomplished without incident. After insertion, the sensor system was successfully uncaged. The constant velocity test on Rev 2 and the health check on Rev 4 were also accomplished successfully.

Operational photography began on Rev 5, Mission Op No. 4, and continued with no camera system malfunctions until Rev 980 when the system failed to execute two operations. The failure was determined to be a missing forward camera take-up Builder Roller (BR) down verification interlock signal. Operations were resumed on Rev 996 with the system configured in SCC II with BR down verification interlock disabled (VIA-DIS). When transfer to RV-4 was made, VIA was re-enabled and operated satisfactorily for the remaining portion of the mission.

In top seems

With subsequent Vendor data the nitrogen gas leak, detected on the pad, was isolated to the low pressure side of the regulator and calculations showed the magnitude of the leak would not cause any significant increase in gas usage rate. On Rev 563 the HPIV-A was opened and the pneumatics system remained in it's normal configuration for the remaining portion of the mission.

On Rev 1268 the system shut down due to a failure of the aft camera take-up integrator servo to reset at TU brakes off. This failure necessitated eliminating nested operations when operations were resumed on Rev 1300. The system continued to operate normally for the rest of the mission.

Evaluation of the RV-I film indicated a need to change the forward camera focal plane plus 8 microns and the aft camera in-track OOAA setting minus 3 steps. These changes were made on mission ops 156 and 160 respectively. Evaluation of the RV-2 film indicated a need to change the forward camera cross-track OOAA bias by plus I step. This change was accomplished on mission OP 399.

The aft camera film supply contained one 2600 foot segment of SO-255 color film and one 3000 foot segment of FE-3916 IR color film. The operational intervals associated with the color films were as follows:

SO-255 OPS 723 to 747 Revs [51] to 1596 FE-3916 OPS 748 to 774 Revs [597 to 1694

The active photographic mission was terminated with RV-4 recovery on day 105 following depletion of both film supplies. A solo phase of the mission extended the vehicle life to day 109, at which time the vehicle was deboosted and re-entered.

1.3 Mission Highlights

Sensor system highlights of the mission can be summarized as follows:

- The sensor system demonstrated a functional orbital life of 105 days.
- b. Both forward and aft cameras utilized 100% of their respectative film supplies. Approximately 95% of the available pneumatics was expended.



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1.3 Mission Highlights - Cont'd.

c. The sensor system demonstrated the capability to operate satisfactorily with FE-3916 infrared color film and S0-255 color film in the aft camera.

4	
A	
La a	

e. The general over-all mission image quality for both cameras ranged from very good to poor; the poor being attributable to atmospheric conditions, high sun angles and specular/shadowless acquisitions. Majority of the good imagery was associated with the aft camera.

Figure I-I presents a graphic history of remaining system life percentages throughout the mission.

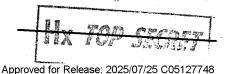
1.4 Launch Configuration

- a. Mission Operation Number 1208.
- b. Intra-range Operation No. 6245.
- c. Satellite Vehicle SV-8.
- d. Sensor System S/N Oll.
- e. Sensor System Configuration.

	Forward Camera	Aft Camera
Filter Types	W-12	W-12
Focal Length	59.9760 in.	59.9890 in.
Focus Setting	68 Microns	25 Microns
OOAA Setting		
In-Track	-4 CMD Steps	-2 CMD Steps
Cross-Track	I CMD Step	-3 CMD Steps
Film Type	1414	1414/S0-255/FE-3916
Film Length	108,854	106,567
Film Weight	862.1 lbs.	861.4 lbs.
Spool Number	5077	5076
Pneumatics Loaded	35.4 lbs	5.

1.5 Launch and Orbital Parameters

	Planned	<u>Actual</u>
Launch Time-GMT	2020Z	2020Z
Launch Time-SVT	67.0	67.0
Inclination-degrees	94.51	94.52



1.5 Launch and Orbital Parameters-Cont'd.

	Planned	<u>Actual</u>
Initial Perigee-n. miles	84.94	85.55
Initial Apogee-n. miles	162.22	164.73
Argument of Perigee-		
degrees	149.71	141.36
Initial Period-minutes	89.0	89.01

Table 1-1 and Figures 1-2 and 1-3 define the basic orbital parameter considerations for the active mission. Forty-three orbit adjusts were performed.

1.6 Mission Film Usage Summary

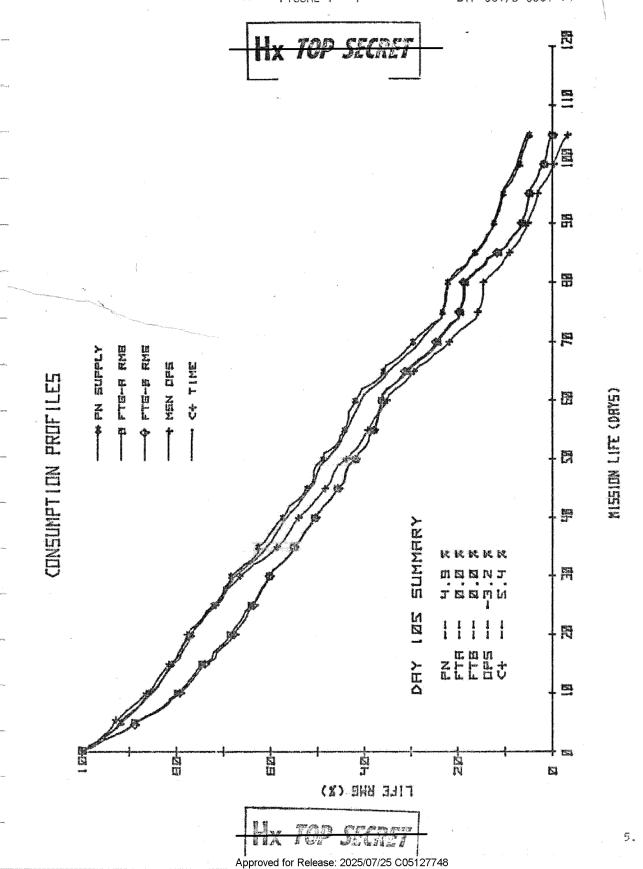
The distribution of film footage as functions of the various operating modes is presented in Figures I-4 to I-21. The mission segment to segment film usage is summarized as follows:

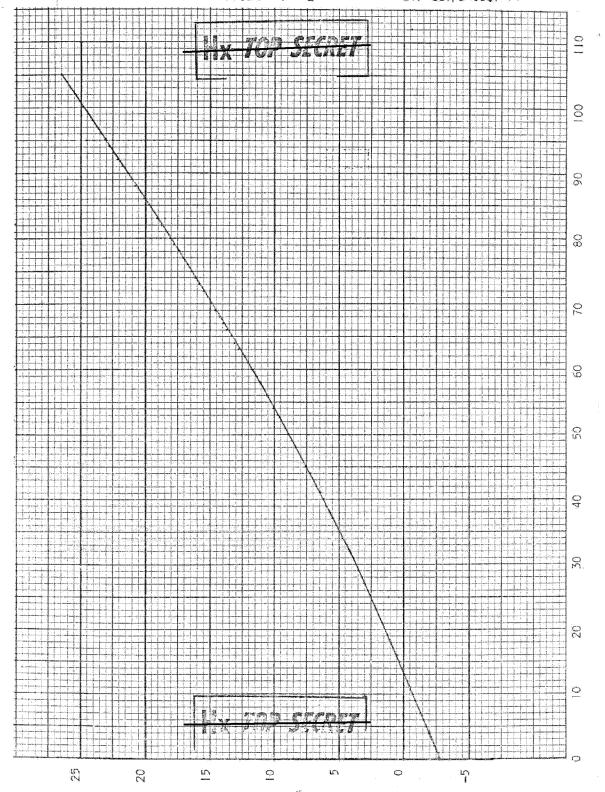
	Rev Span	Camera	Recovered Footage
RV-I	Launch-225	Forward Aft	28042 28111
RV-2	226-674	Forward Aft	28848 27766
RV-3	675-1116	Forward Aft	25258 24225
RV-4	1117-1700	Forward Aft	26827 26608

Of this footage, the engineering and other non-intelligence operations consumed approximately 4600 and 4800 feet for the A and B sides, respectively, as summarized in the following:

1208 Non	-Intelligence	
den .	Forward Camera	Aft Camera
Pre-Launch	1853	1991
RV-I Engineering	1055	1055
RV-2 Engineering	702	702
RV-3 Engineering	437	478
RV-4 Engineering	596	605
Total Utilization	4643	4831
Film Recovered	108975	106710
PCT. Non-Intelligence	4.26	4.53

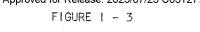
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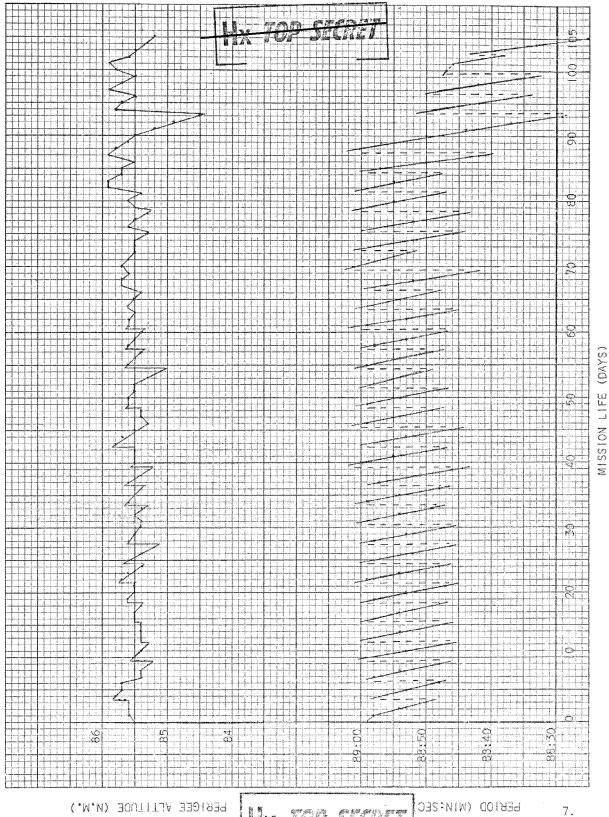




BETA ANGLE (DEGREES)

| S X S TO THE CENTIMETER 18 X 24 CM. REUFFEL & ESSER CO.





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TABLE I - I

BASIC ORBITAL PARAMETERS

DAY	REV	PERIOD	PERIGEE	APOGEE	TNC	ARG/PER	B ANG
_	Limit 4	00 50		120.0	A	1.4-7.4	
0	NOM	88:59	85.5	162.9	94.5	143.4	. 75 %
0	1	89:00	85.5	164.5	94.5		-2.6
2	8 24	88:58 88:54	85.6 85.6	163.5 161.0	94.5	138.9 134.8	-2.6 -2.3
3	40	88:50	85.6	158.4	94.5 94.5	130.6	-2.3 -2.1
0A#1	46	00:00	02.0	120.4	94.0	120.0	-2.1
4	57	88:57	85.8	165.1	94.5	130.9	-1.9
.5	73	88:53	85.7	162.7	94.5	126.7	-1.7
6	89	88:48	85.7	160.1	94.5	122.7	-1.5
OA#2	94	.00,40	05.1	.10031	27.4.2	1 Am Em #- 1	1.4.2
OA#3	96						
7	105	88:58	85.4	161.1	94.5	147.5	-1.3
8	121	88:54	85.4	158.5	94.5	143.2	-1.1
9	138	88:48	85.3	155.0	94.5	138.4	-0.9
OA#4	143						
10	156	88:58	85.5	162.4	94.5	140.4	-0.7
1	170	88:53	85.4	159.5	94.5		-0.5
12	186	88:47	85.3	156.5	94.5	132.0	-0.3
OA#5	192		ă.				
13	202	88:58	85.4	165.4	94.5	133.9	-0.1
14	218	88:54	85.4	162.5	94.5	129.8	+0.1
15	235	88:48	85.4	159.1	94.5	125.3	+0.3
0A#6	240						
0A#7	242	00 50	AT	160 7	63.5	1.47 0	Λ 6
16	251	88:58	85.5	160.7	94.5	147.2 143.0	0.5
17	267 283	88:54	85.5 85.4	158.0 155.2	94.5 94.5	138.8	1.0
18	∠65 289	88:49	00.4	193.Z	94.0	1,20.0	10
0A#8 19	299	88:58	85.6	162.7	94.5	140.1	1.2
20	313	88:53	85.5	160.2	94.5	135.5	1.4
21	332	88:47	85.5	156.3	94.5	131.2	1.6
OA#9	337	ωφ. _ε	92,2	150.5	J	1.20 1.4.22	
22	348	88:59	85.7	166.2	94.5	133.4	1.9
23	364	88:54	85.6	163.1	94.5	129.6	2.1
24	380	88:48	85.4	159.5	94.5	125.5	2.3
OA#10	386						
0A#11	388						
25	397	88:58	85.6	160.3	94.5	147.2	2.5
26	413	88:52	85.4	157.2	94.5	142.8	2.7
27	429	88;47	85.2	154.2	94.5	138.4	3.0
OA#12	434						

TABLE i - 1 Cont'd.

BASIC ORBITAL PARAMETERS

DAY	REV	PERIOD	PERIGEE	APOGEE	INC	ARG/PER	B ANG
28 29 30 0A#13	445 461 477 483	88:58 88:53 88:47	85.6 85.5 85.4	162.0 159.1 155.8	94.5 94.5 94.5	141.8 137.6 133.3	3.2 3.5 3.7
31 32 33 0A#14	494 510 526 532	88:59 88:54 88:49	85.4 85.5 85.4	165.3 162.5 159.5	94.5 94.5 94.5	135.4 131.1 127.0	3.9 4.2 4.4
OA#15 34 35 36 OA#16	534 542 558 575 580	88:59 88:54 88:48	85.6 85.5 85.4	161.0 158.3 154.6	94.5 94.5 94.5	147.9 143.5 138.8	4.7 4.9 5.2
37 38 39 0A#17	591 607 623	88:57 88:51 88:46	85.6 85.4 85.3	161.8 158.6 155.4	94.5 94.5 94.5	140.7 136.5 132.3	5.5 5.7 6.0
40 41 42 0A#18	639 655 672 683	89:00 88:55 88:50	85.5 85.5 85.5	166.3 163.4 160.4	94.5 94.5 94.5	135.6 131.4 126.9	6.2 6.5 6.8
43 44 45 0A#19	688 704 720 726	88:58 88:53 88:46	85.8 85.7 85.5	166.6 163.3 159.5	94.5 94.5 94.5	128.3 124.3 120.4	7.0 7.3 7.6
OA#20 46 47 48 OA#21	728 736 753 769 774	88:59 88:54 88:49	85.3 85.4 85.4	161.9 158.7 155.7	94.5 94.5 94.5	148.5 143.6 139.2	7.8 8.1 8.4
49 50 51 OA#22	785 805 817 823	88:59 88:49 88:48	85.6 85.5	163.0 160.1 156.6	94.5 94.5 94.5	141.1 136.9 132.7	8.6 8.9 9.2
52 53 54 0A#23 55	834 850 866 871 882	88:58 88:52 88:51 88:59	85.5 85.3 85.1	164.9 161.3 157.7	94.5 94.5 94.5	133.8 129.6 125.5	9.5 9.8 10.1
56 57	896 914	88:54 88:49	85.5 85.4	164.3 160.8	94.5 94.5 94.5	129.6 125.5 121.4	10.3 10.6 10.9

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TABLE I - I Cont'd.

BASIC ORBITAL PARAMETERS

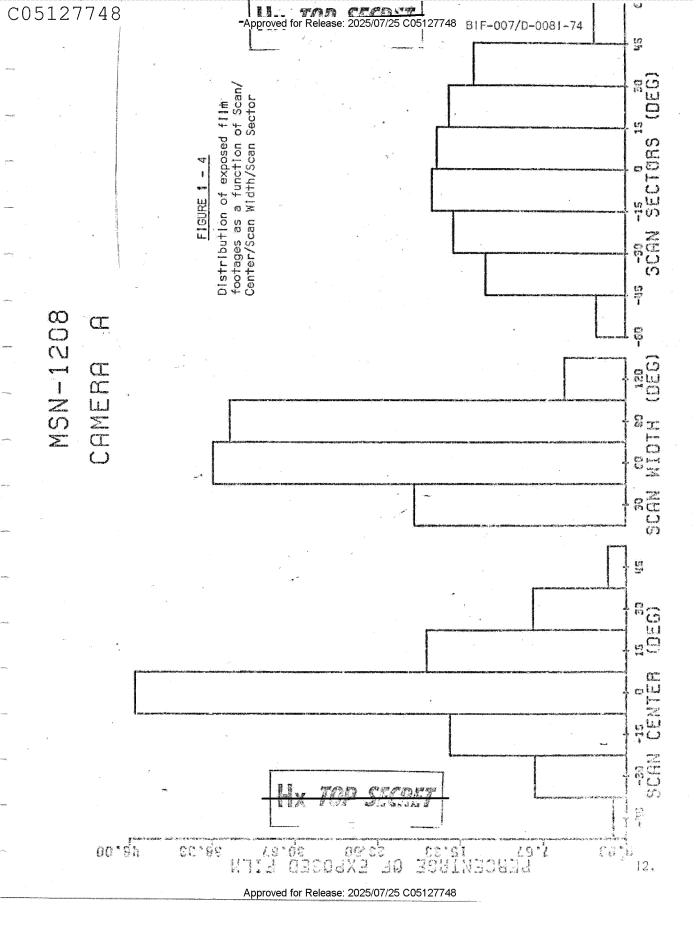
DAY	REV	PERIOD	PERIGEE	APOGEE	INC	ARG/PER	B ANG
OA#24	920						
0A#25	922						
58	931	88:58	85.6	160.6	94.5	147.6	11.2
59	947	88:53	85.5	157.8	94.5	143.1	11.5
60	963	88:48	85.4	154.9	94.5	138.7	11.8
00 0A#26	975	00:40	0.7.4	. 1.74.7	34.3	1001	11.0
61	979	88:59	85.6	162.9	94.5	142.5	12.1
62	996	88:53	85.6	159.5	94.5	138.2	12.4
63	1012	88:47	85.5	155.4	94.5	133.5	12.8
	1012	00147	۵۰,۲۵	177.4	24.2	100.0	12.0
0A#27		00.50	05 6	165.5	94.5	136.4	13.1
65	1029 1644	88:59 88:54	85.6 85.5	162.2	94.4	132.2	13.4
66	1060			158.7	94.4	128.1	13.7
00 0A#28	1065	88:49	85.4	130.7	94.4	120.1	1
67	1005	88:57		165.2	94.4	130.2	14.0
68	1076	88:52	85.7	165.2	94.4	126.1	14.3
69	11092	88:44	85.6	156.8	94.4	121.5	14.6
09 0A#29	1120	00:44	62.0	120.0	94.4	(21.5	15.0
70	1125	89:06	85.7	174.1	94.5	127.0	14.9
70	1141	88:59	85.6	169.8	94.5	122.8	15.2
72	1157	88:53	85.5	165.9	94.4	118.9	15.5
0A#30	1162	00:33	٠,٠٠٥	102.5	24.4	110.3	في ∓ في: ا
0A#30 0A#31	1164			4			
73	1173	88:58	85.5	160.2	94.4	147.7	15.9
74	1190	88:52	85.5	157.0	94.4	143.0	16.2
75 75	1206	88:46	85 _* 3	153.5	94.4	138.5	16.5
OA#32	1211	00:40	ر∡رن	122.0	2014 M	1 20 . 2.	1947
76	1222	88:57	85.6	161.8	94.4	141.1	16.8
77	1238	88:52	85.5	158.7	94.4	137.0	17.1
78	1254	88:45	85.3	154.1	94.4	132.8	17.4
0A#33	1260	00147	02*2	3 27-4-4 3	271	122.0	1,197
79	1270	88:59	85.5	164.9	94.4	137.5	17.8
0A#34	1282	00:09	.05.5	104.9	27.4	12/2	17.0
80	1286	88:55	85.6	162.3	94.4	134.1	18.1
81	1303	88:49	85.4	158.5	94.4	129.9	18.4
OA#35	1313	00,49	02.4	12042	2 mi * mi	14.2 + 2	10.4**
82	1321	88:59	85.9	166.2	94.4	133.0	18.8
83	1335	88:55	85.9	163.3	94.4	129.3	19.1
84	1351	88:49	85.7	159.5	94.4	125.2	19.4
04#36	1357	00173	92. I	12282	J19 6:19	127.6	12.67
85	1368	88:57	85.7	167.3	94.4	125.9	19.8
			ngt gat 19 9	1.40 5 9 -0"	≫ '7 • '7'	1.2.4 1.2	1940

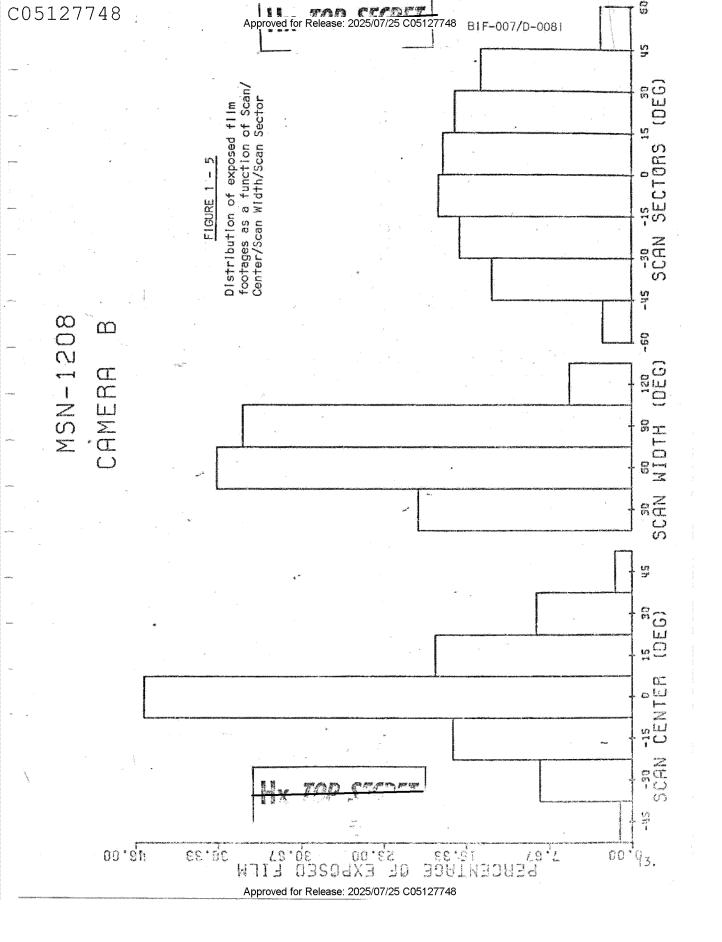
Hx 100 SECRET

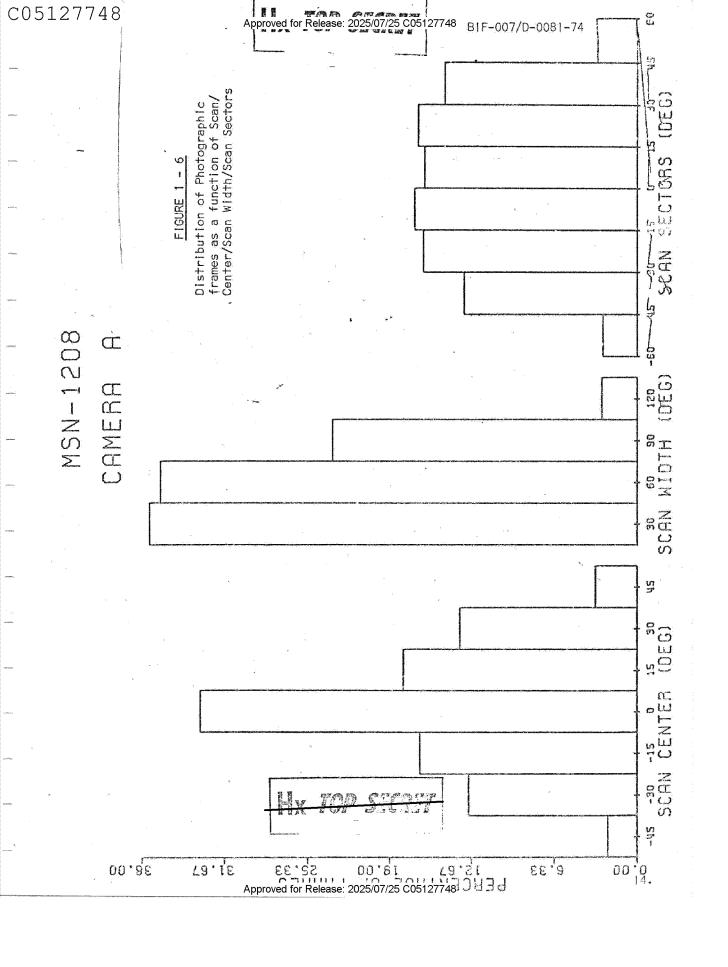
TABLE I - I Cont'd.

BASIC ORBITAL PARAMETERS

	DAY	REV	PERTOD	PERIGEE	APOGEE	INC	ARG/PER	B ANG
	86	1384	88:50	85.5	162.8	94.4	121.8	20.1
	87	1400	88:42	84.9	156.8	94.4	117.6	20.4
	OA#37	1406		7.75	,			
	OA#38	1408						
	88	1416	89:02	85.8	164.3	94.4	148.0	20.8
	89	1432	88:57	85.6	160.7	94.4	143.6	21.1
	90	1449	88:50	85.5	156.3	94.4	138.0	21.4
	91	1465	88:44	85.2	152.3	94.4	134.4	21.8
	92	1481	88:37	84.9	147.8	94.4	129.9	22.1
	93	1497	88:29	84.5	142.9	94.4	125.5	22.4
	OA#39	1502						
	94	1513	88:49	85.8	155.1	94.4	138.0	22.8
	95	1530	88:42	85.7	151.2	94.4	133.2	23.1
	96	1546	88:36	85.5	147.2	94.4	128.8	23.4
	OA#40	1551	F					
	97	1562	88:48	85.9	155.1	94.4	134.3	23.8
	98	1578	88:42	85.7	151.3	94.4	130.0	24.1
	99.	1594	88:35	85.5	147.2	94.4	125.7	24.4
1	OA#41	1600	ė.					
	100	1611	88:47	85.8	156.1	94.4	130.3	24.8
	OA#42	1616						
	101	1627	88:46	85.9	155.6	94.4	128.6	25.1
	102	1643	88:39	85.6	151.8	94.4	124.6	25.4
	OA#43	1649						
	103	1659	88:41	85.5	153.1	94.4	123.9	25.8
	104	1676	88:33	85.2	148.3	94.4	119.3	26.1
	105	1692	88:24	84.3	141.4	94.4	115.0	26.5







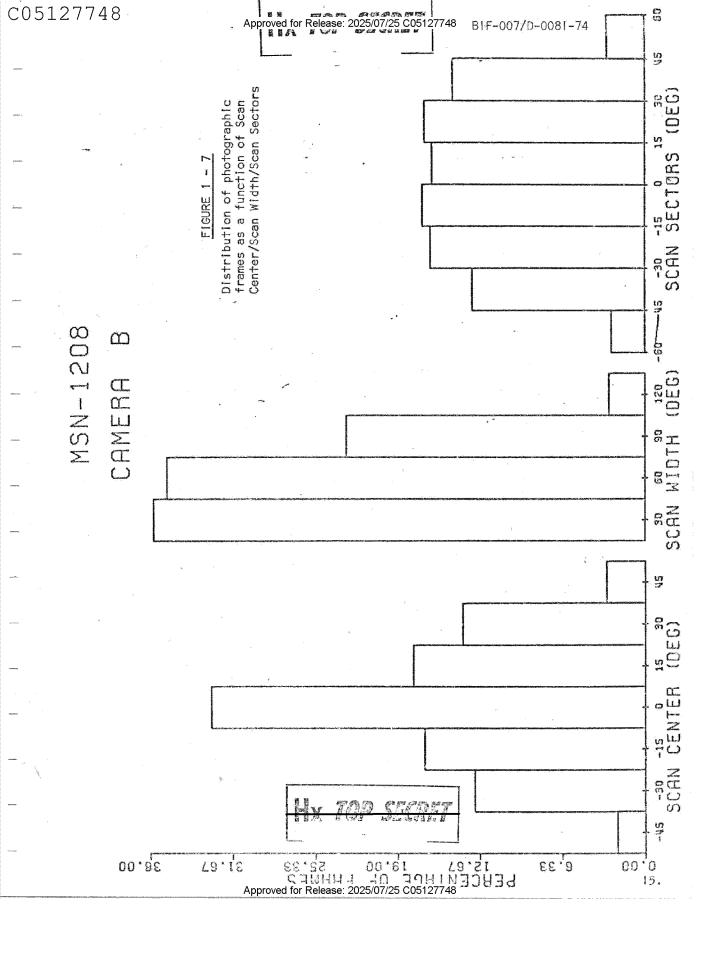


FIGURE 1 - 8

Distribution of land mass coverage as a function of Scan Sectors



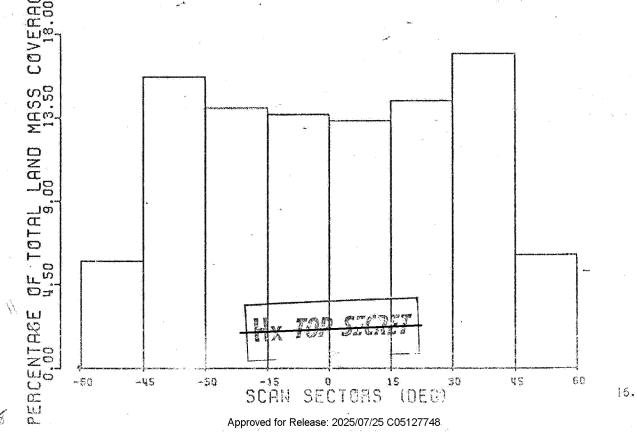
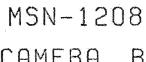
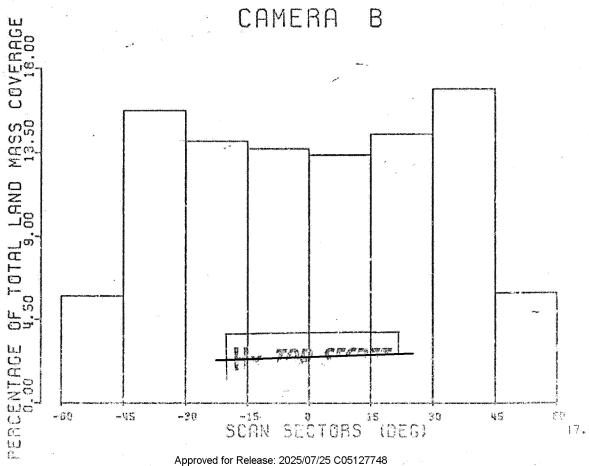
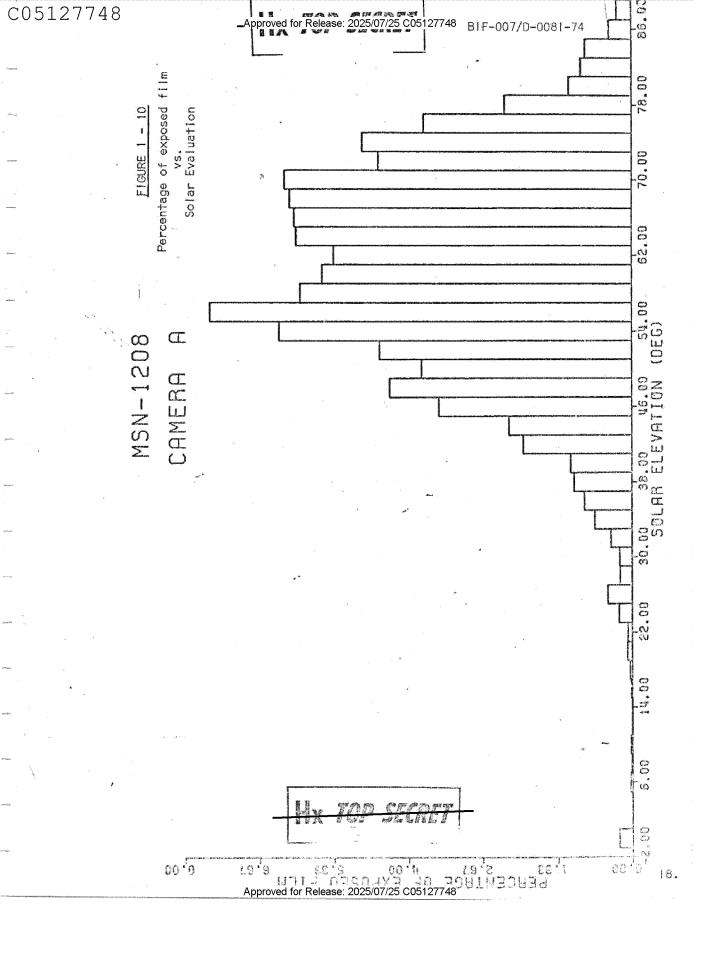


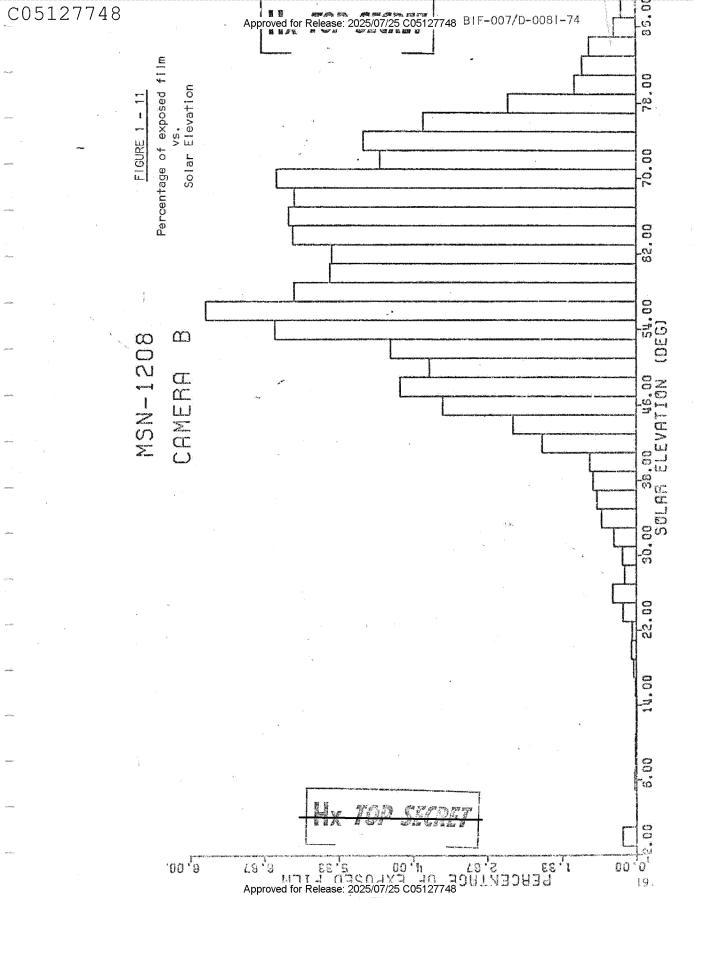
FIGURE 1 - 9

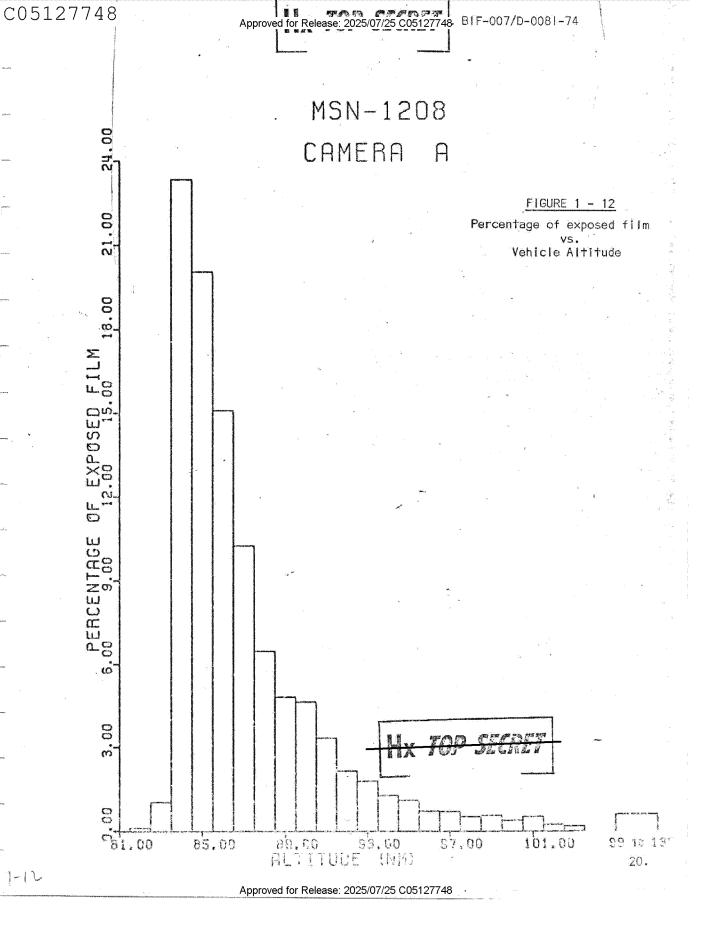
Distribution of land mass coverage as a function of Scan Sectors

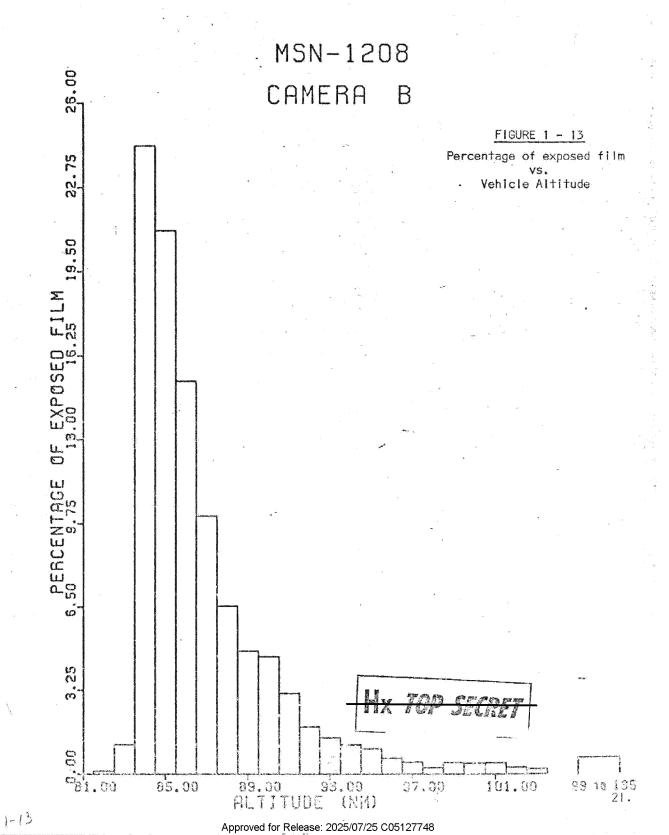












15.75

13.50

OF EXPOSED FILM

PERCENTAGE

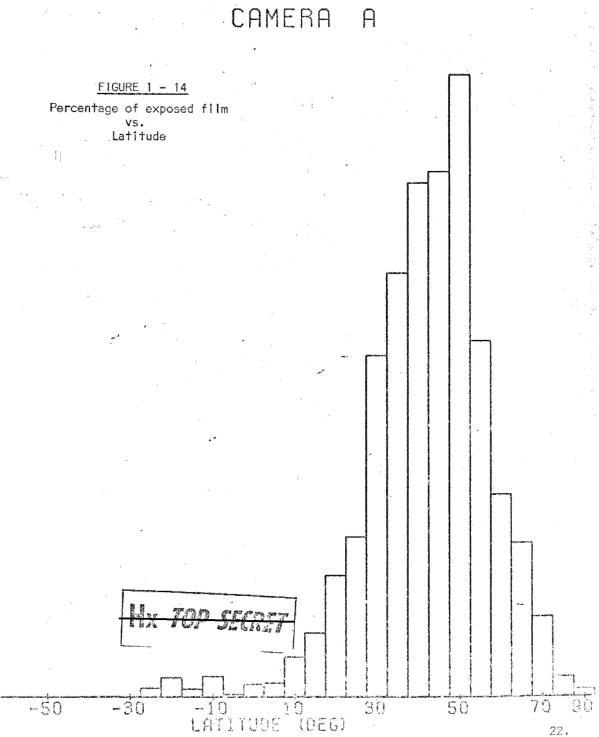
2 2

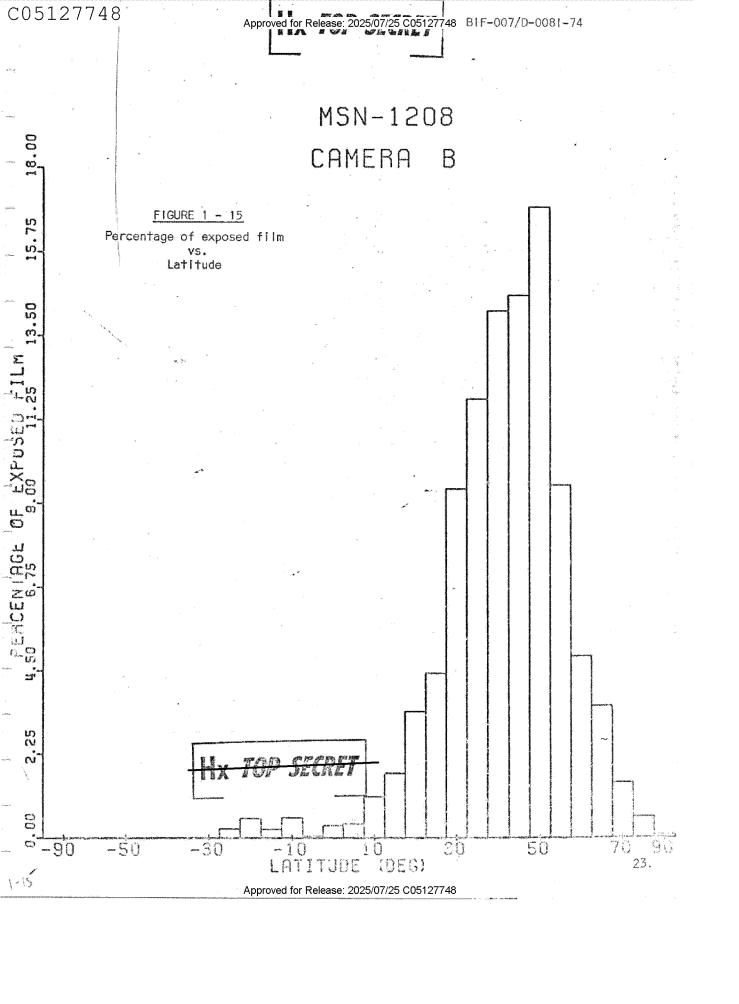
0.00

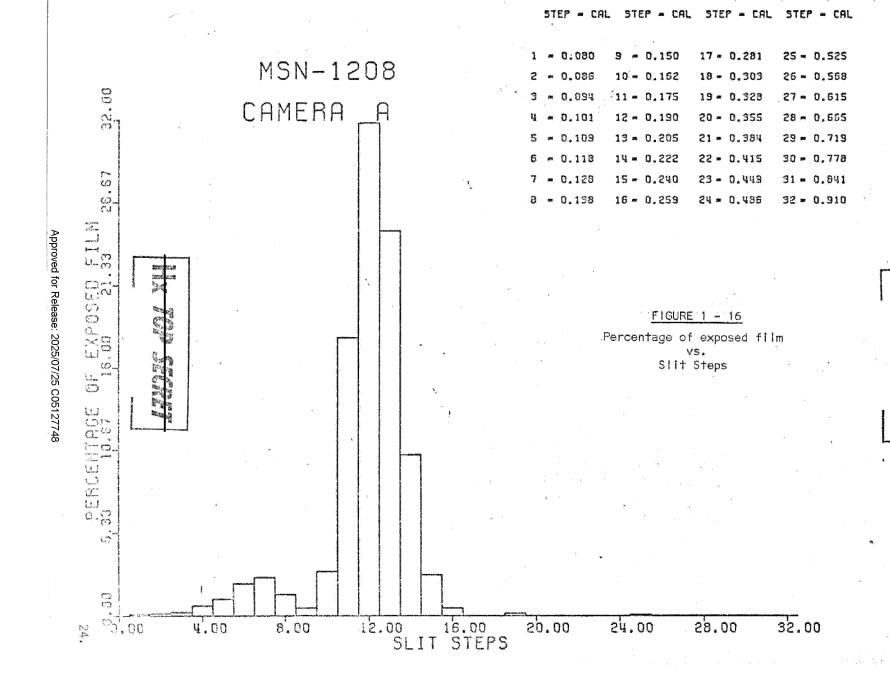
1-1-

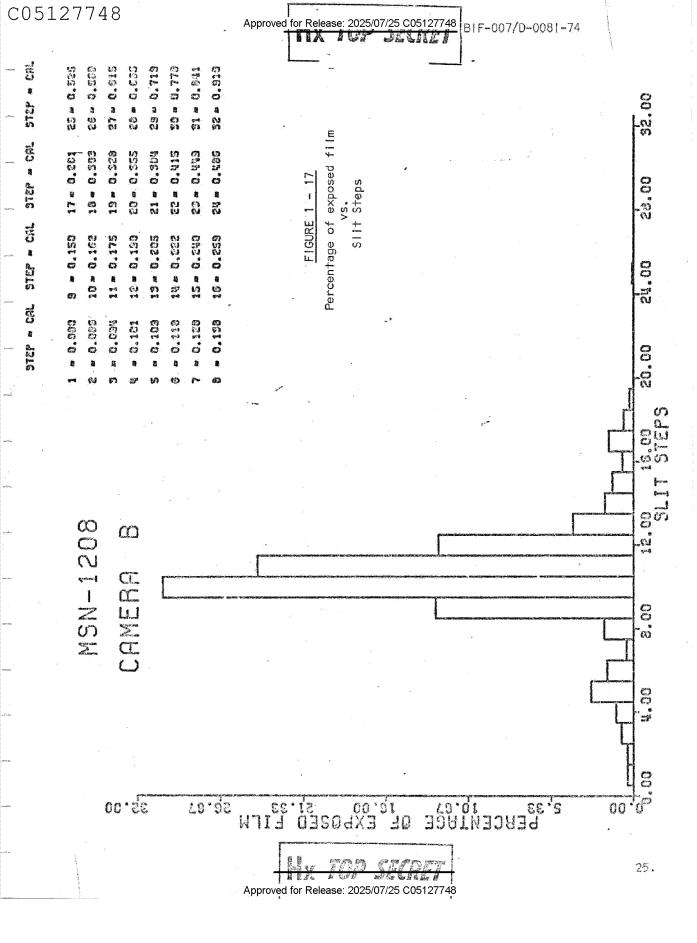
-90







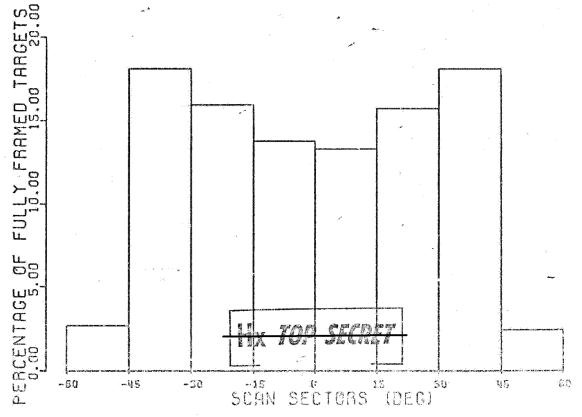




26.

Distribution of fully framed Targets vs. Scan Sectors

MSN-1208 CAMERA

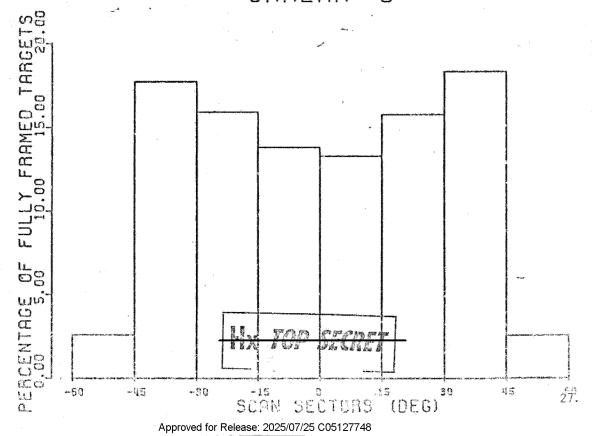


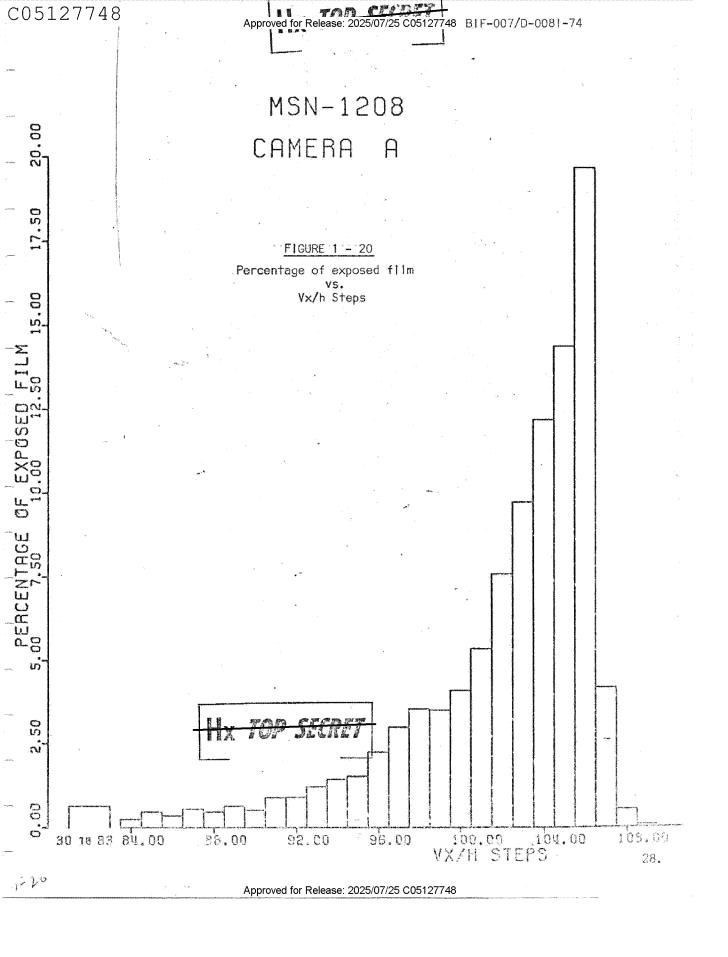
1-19.

FIGURE 1 - 19

Distribution of fully framed Targets vs. Scan Centers

MSN-1208 CAMERA B



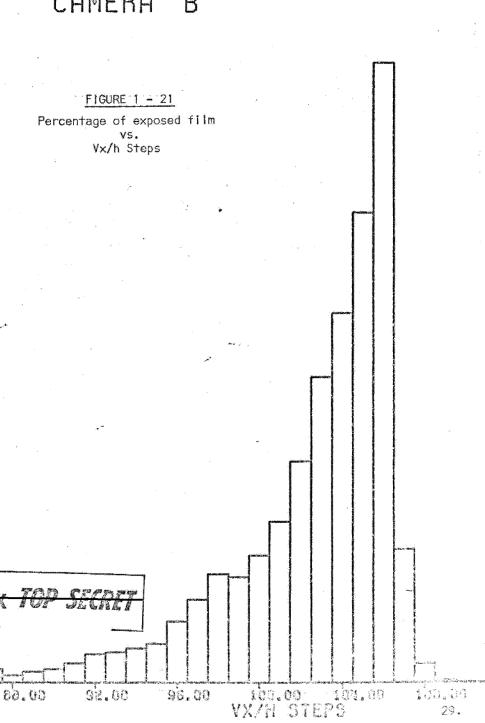


(S)

S. SO PENCENTHGE OF EXPUSED FILM

30 to 82 84.00

MSN-1208 CAMERA B



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2.0 SENSOR SYSTEM PERFORMANCE

2.1. Coarse Film Path

Coarse film path diagnostics indicated nominal performance throughout take-ups one, two and three. Analysis of a B-side emergency shut down (ESDB), which occurred during take-up four operations, indicated a hardware failure in the coarse path control electronics.

The ESDB occurred on the start-up of an operation planned for Rev 1268 and was due to a low tension condition in the coarse path. A B-side creep test conducted over 1283 Pogo also shut down, but this shutdown was due to a high tension coarse path condition.

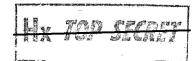
Analysis of the Rev I268 ESDB and primarily of the Rev I283 ESDB indicated that the take-up integrator reset signal to the take-up servo loop was not operating. The Rev I268 data was in telemetry mode C, as is most operational payload data, and the take-up integrator output signal is not included in the telemetry format. The Rev I283 data was in telemetry mode B which does include the take-up integrator output signal.

The take-up integrator integrates the output coarse tension error from nominal and modifies the take-up servo error signal, which is also a function of the velocity command, velocity feedback and the coarse output tension offset. The take-up servo responds by altering the take-up velocity in a manner consistent with correcting the output coarse tension error.

Integration of the tension error begins at camera power turn-on. There is a small tension error at the start-up of most camera operations, and because of the nominal time delay between camera power on (CB+) and film transparts on (FT+), the integrator out-put at the time the take-up brakes are released can be substantial. Therefore, the integrator output is reset to null upon application of brake release power via the 35ms. reset signal generated within the take-up electronics.

In the absence of the reset signal, the integrator output will erroneously alter the error signal to the servo loop. The magnitude of the error introduced is dependent on the original coarse output tension offset and the time duration between camera power on and transports on.

In the case of the Rev 1268 ESDB, the CB+ to FT+ time was in excess of 120 seconds for film path pressurization purposes, and although the initial coarse tension offset was small, the integrator output was saturated by the time brakes released and indicative



of a much larger over tension condition than what actually existed. The servo loop therefore overcorrected for the actual tension error and subsequently caused the under tension ESDB. The Rev 1283 ESDB resulted when the servo overcorrected for an initial undertension condition and drove the system into the high tension state.

Analysis of coarse tension data from currently available station tapes indicated integrator failure occurred between operations 598 and 605. Under normal operating conditions (i.e. initial coarse output tension greater than 2.2 lbs. and less than 2.8 lbs; CB+ to FT+ less than or equal to 17 seconds) the TU servo can recover from the integrator error present at brake release without the reset signal. The remainder of take-up four operations were constrained to a maximum C+ to FT+ time of 17 seconds and the startup coarse output tension limits noted above. No further problems in this area were encountered.

2.2 Fine Film Path

Fine film path diagnostics indicated proper hardware performance throughout the mission for both camera systems.

2.3 Command and Control

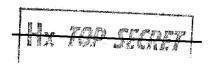
The sensor system performance with respect to the Command and Control Subsystem was nominal throughout the mission. All commands were properly received and executed.

2.4 Sensor System Control

On Rev 980 the sensor system failed to execute the second and third of three non-nested operations. The first operation, Msn OP 490, executed normally.

The set-up commands for the two Ops that failed to execute, up to and including seal doors open, were properly executed. Neither the SU nor the TU brakes were released and the film transports did not operate.

On Rev 989 both an A-Side and a B-Side CV test were run with verification interlocks enabled. The A-Side test failed to execute. The B-Side test executed normally. On Rev 991 an A-Side CV test was successfully executed with verification interlocks disabled.



On Rev 993 an A-Side CV test was run with SCC-II and verification interlocks disabled. This test also failed to execute which isolated the problem to the A-Side verification circuitry external to either SCC I or SCC II. The most probable suspect for the failure was an absence of the "Builder Roller Down" verify signal.

On Rev 995 a health check was successfully executed in SCC II with VIA disabled. Stereo operations were resumed on Rev 996 using SCC II with VIA disabled and continued without further problems through the remainder of RV-3.

When transfer to RV-4 was made, VIA was re-enabled and the mission successfully completed in that configuration with SCC II.

Upon receipt of the RV at Rochester, the outer shrouds were removed and a visual inspection was made with an infrared scope and infrared photographs were taken. Both the visual inspection and the photographs indicated that the condition of all portions of the Builder Roller and the lower verify switch were normal. Extensive electromechanical testing did not provide any information to help isolate the cause of the Builder Roller Verify signal failure.

2.5 Optical Bar Performance

The Optical Bars performed properly throughout the mission. Variations between commanded and actual OB velocities were no different than those noted during pre-flight systems test and were within the specification limits of .00054 rad/sec.

2.6 LSFS/Focus

Mission 1208 used pre-flight determined focus settings for 1414 black and white film, SO-255 color film and FE-3916 infrared film.

The forward camera was set at a nominal of 68 microns through RV-1. Image quality evaluation of the returned film resulted in a change to a new nominal of 76 microns commencing with Msn Op 156 in RV-2 and continuing through the remainder of the mission.

The aft camera was set to a nominal of 25 microns for 1414 material and 55 microns for both SO-255 and FE-3916. No readjustments from the pre-flight planned values were required.

The LSFS output, as with 1207, was deemed reliable only on the first operation of each day (i.e., after three hours of non-operation and during the first five minutes of the first subsequent OP). Readings of the LSFS output were taken only at these times throughout mission 1208.

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2.7 Instrumentation

All instrumentation operated normally throughout the mission. The system provided consistent and accurate data for analysis of anomaly conditions and for the routine verification of camera status. Although not part of the sensor system instrumentation system, a MUX failure necessitated switching from the primary (MUX 4A) to the backup (MUX 4B) unit.

2.8 Pneumatics

The pneumatic system nitrogen reserve status for mission 1208 was as follows:

		TANK	A	TANK B					
<u>Event</u>	Press. (psi)	Temp	Mass (lbs)	Press (ps1)	Temp (°f)	Mass (lbs)	Total Mass (Ibs)		
Liftoff	3388	69	17.8	3374	68	17.7	35.5		
End of Primary Mission	196	69	1.1	210	67	1.2	2.3		

Toward the end of the mission it became necessary to manage camera operation in terms of the distribution of scan centers, scan lengths and frame count to avoid the possibility of depleting the gas supply prior to the total usage of the film supply. The computed PN+ use rate was a constant 0.023 lbs/min throughout the mission.

2.8.1 During the launch countdown, on Day R-1, the A side regulated pressure was observed to decay at an abnormally high rate, e.g., from 2.46 to 1.28 psi in 300 seconds. On the basis of this decay rate and the immediately available design data, several hundred manufacturing drawings, pertaining to the pneumatic system plumbing volumes, it was concluded that a leak had developed on the high pressure side of the regulator and was of sufficient magnitude to be unacceptable for flight operation, i.e., the continuous loss of gas would severely shorten the mission. An acceptable corrective action was taken by isolating the leak from the high pressure gas supply, tank pressure, by commanding the A side high pressure isolation valve (HPIV-A) to the closed position following the uncage and OB stow sequences executed on Rev 0. The only disadvantage to this configuration was a reduction in system reliability as a result of the loss of parallel redundancy in the D bar gas supply.



Subsequent to the launch, the plumbing system volumes were measured at the supplier's facility and determined to be significantly different from the values calculated from drawings. (The measured values were: high pressure stage = 0.290in³, intermediate pressure stage = 0.036in³, low pressure stage = 3.085in³.) New analysis were performed and it was concluded that the leak was on the low pressure side of the regulator and was of negligible magnitude. Therefore, it was decided to open the HPIV-A to regain maximum system reliability.

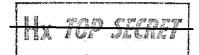
As a precaution, on orbit tests were performed to verify that the leak was in the low pressure stage. The tests were conducted by momentarily opening the HPIV-A and monitoring the regulated pressure decay rate following valve closure. As a result of the analysis and tests, the HPIV-A was opened on Rev 563 and left open for the remainder of the mission.

A detailed analysis of the pneumatics system leak is provided in. "Memorandum #930, OTD, SED, SAE, To:
dated:

2 May 1974.

2.8.2 Path Pressurization

For the first time in eight missions it became necessary to acuate the pneumatic system operate valves to maintain the film path pressure above the ballooning criterion. The initial repressurization occurred after transfer to TU-4 and was repeated as required for the nemainder of the mission. Although the path leak rate was within specification requirements, the combination of short operations with corresponding small increases in path pressure, separated by long quiescent periods caused the repeated occurrence of the low pressure condition. To minimize the additional gas usage, a procedure was used wherein the path was repressurized, increased by approximately 0.1 psi, only at those times the path pressure had decayed to the ballooning pressure limit.



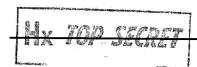
BIF-007/D-0081-74

2.9 Trend Analysis

A statistical trend analysis of sensor system performance was maintained by the Systems Integration Section throughout mission 1208. Data samples were taken from one operation per day, when available, and mean values and standard deviations were calculated and plotted for selected functions to facilitate the detection of any long term trands that would indicate the orbit of system degradation. The analysis indicated a momentary disturbance in all tension sensors and the A side metering capstan summed error in the first 12 scan degrees of operation 564, however, the signals returned to nominal values for the remainder of the operation. Although not regarded as a trend or anomaly, the B side metering capstan summed error mean valve shifted from 0.034 oz. in. with 1414 material to approximately 0.043 oz. in. with \$0-255 film. The mean level returned to approximately 0.034 oz. in. with FE3916 film. Otherwise, all system functions remained nominal throughout the mission with no indication of abnormal long term trend.

The functional parameters used for the analysis were as follows:

- 1. Film to Bar Sync Velocity Error (P451, P452)
- 2. Metering Capstan Summed Error (P403, P404)
- 3. Platen Skew Error (P415, P416)
- 4. Platen Photo Summer Error (P411, P412)
- 5. Input Drive Capstan Summed Error (P803, P804)
- 6. Output Drive Capstan Summed Error (P811, P812)
- 7. Supply Drive Summed Error (P105, P106)
- 8. Take-up in Use Drive Summed Error (TSEA, TSEB)
- 9. Optical Bar Summed Error (P501, P502)
- 10. OB Velocity Error
- 11. Looper Position (P601, P602)
- 12. Film Path Carriage Position (P713, P714)
- 13. Take-up Carriage Position (P951, P952)



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3.0 MISSION EVENT HISTORY

A summary listing of all sensor system photographic operations is presented in Appendix A-I of this report. The summary primarily covers operational photography, but also includes PFA engineering photography. The following is a chronological description of these engineering operations plus other special events that occurred during Mission 1208.

3.1 Ascent

The countdown and launch were accomplished without incident, with uncage (sequences 204 and 205) and OB stow (sequences 213 and 214) occurring in a normal manner following BV-SV separation. These events were verified from tape recorder playback at Rev 1 POGO.

3.2 Health Checks

Day I operations through Rev 4 were designed to verify system health and confirm orbit operational readiness. An engineering operation designed as a baseline test was performed on Rev 8. The health check events were as follows:

- Rev I: An uncage verification check, sequence 215, was performed over POGO to confirm the uncage event.
- Rev 2: A constant velocity run, sequence 208, was performed over KODI. This was the first attempt to transport film after launch. The Sensor System worked properly, and the film was correctly aligned within the film path. Steerers, tensions, and take-up and supply drive summed errors were well within limits.
- Rev 4: The sensor system health check, sequence 175, was performed over POGO. All sensor system executed commands were functionally verified, including all fested bits of the variable commands. Focal plane position indicated 68 microns for the forward camera, and 25 microns for the aft camera.
- Rev 8: A scheduled engineering operation, sequence 209, was performed over COOK to provide characteristic telemetry data for comparison with data from any future identical functional check. In the event of an anomaly, the telemetry signatures of the two runs could then be equated and any suspected system degradation determined.

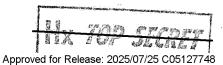
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36.

3.3 Engineering Events

Eleven engineering tests were defined in the SV-8 Engineering Photography Plan. This series of tests were designed to acquire data for assessment of on-orbit camera, lens and film performance. Following is a summary of the tests and their objectives:

	Test	Objective/Status
l.	Thru-Focus (1414)	Optimize Focus. Fully accomplished; confirmed focus (1414) was optimum in RV-2.
3.A	Smear Slits (1414)	Validate Image Motion Compensation settings. Completed in RV-2.
3 . B	Smear Slits (SO255)	Evaluate smear slit for validating image motion compensation settings with color film. Completed in RV-4.
3.C	Smear Slits (FE3916)	Evaluate smear slit for validating image motion compensation settings with IR film. Completed in RV-4.
4.	Color Corn Acquisitions	Evaluate and radiometrically call- brate SO-255. Satisfactorily completed in RV-4.
5.	IR Color Corn Acqui- sitions	Evaluate image quality of FE3916. Accomplished in RV-4.
6.	Lens MTF (1414)	Measure on-orbit lens MTF. Completed in RV-3.
7	Tucson Acquisition	Standard scene for quality assessment. Satisfied in RV-1,2,3 and 4.
8.	Color Thru-Focus (SO-255)	Optimize Focus. Completed in RV-4.
9.	Tri-Bars for Resolution	Photo quality assessment. Satisfied RV-1,2,3 and 4. Acquisitions common with Test 7.
10.	Smear versus Scan Angle (1414)	Assess smear as a function of scan angle location. Fully accomplished. Completed in RV-3.
12.	Dense Culture Acquisition (1414)	Photo/EM correlation. Satisfied in RV-1,2,3 and 4.



		3.4	Mission	1208-1 5	pecial I	Events			
			REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	
			0.8				UNCAGE/SCC I SEL		
. ,	v		0.8				STOW A/STOW B HPIV A CLOSE		
pprov		4	1				UNCAGE VERIFY		
ed for			2				INHIBITED CV		102
Relea	5		4	1-3			SS HEALTH CHECK		163
se: 20			8	8			SS ENGINEERING		63
Approved for Release: 2025/07/25 C05127748			14	13	· ·	75 75	1414 T/F-8,-16,-8,0,+8,0 BOSTON PROVIDENCE	99 99	. 54
05127748			16	14	1	95	1414 T/F +16,+8,0 SAN DIEGO	90	29
W-3404	***************************************		56	42			PN EQUALIZE		
			81	54	and the second	85 80	1414 T/F-16,-8,0 SACRAMENTO SAN FRANCISCO	95 99	56
			86	55			PN EQUALIZE		
			96	63	3A	70	1414 SMEAR SLITS DALLAS/FT WORTH	99	81

1055

3.4	Mission 1208-1 Special Events-Cont'd.

		1413310	1 1200-1	operar c	VOIII 3	00111 0.		
		REV	OFN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
		97	64	3A.	95	1414 SMEAR SLITS LOS ANGELES	99	
				10	85	1414 SMEAR VS SCAN SAN DIEGO	99	124
io pa		129	84	7,9,12	95	TUCSON W/5T RESO	99	
		144	94	ļ.	85	1414 T/F-8A,0,+8B,0 ATLANTA PN EQUALIZE	99	27
35 SECT	į	160	103	10	85 85	1414 SMEAR VS SCAN BALTIMORE WASHINGTON	99 99	93
		176	114	1 3A	75 75	1414 T/F+16,+8,0,-8,0 NEW YORK 1414 SMEAR SLITS PHILADELPHIA	95 95	121
•		184	115			PN EQUALIZATION		
		225	130		80	1414 T/F+16,+8,0,-8,-16 DETROIT	99	34
		225	131			PROTECTIVE WRAP	e w	108
						1208-1 FOOTAGE		1055
					t	ACCUMULATED FOOTAGE		

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		3.5	Missi	on 1208-2 S	pecial	<u>Events</u>			
			REV	OPN	TEST	PRE WX	EVENT/LOCATION /	VER WX	FTG
			226				TRANSFER TO TU2-PREP I		*
			227				COMPLETE TRANSFER-PREP 2		63
			248	139/141			PN EQUALIZE		
Appro			281	156			PBF A SET TO 76 PER PFA DIRECTION		
ved for R			291				IT-B SET TO -5 STEPS PER PFA DIRECTION		
elease	1 1		313	165/166			PN EQUALIZE		,
Approved for Release: 2025/07/25 C05127748			338	175	12	70	QUALITY VARIABILITY MIAMI	. 75	38
7/25 C			356	187			PN EQUALIZE		
0512			428	224			PN EQUALIZE		
7748			435	228	10 3A	70 70	1414 SMEAR VS SCAN NEW YORK 1414 SMEAR SLITS PHILADELPHIA	80	144
			451	234	3A	70 70	1414 SMEAR SLITS BOSTON PROVIDENCE	99 90	49
			480				LEAK RATE TEST-5 SEC		
			493	254/256			PN EQUALIZE		

1757

		3.5	Mission	1208-2	Special I	Events-C	ont'd.	<i>y</i>		,
			REV	OPN	TEST	PRE WX	EVENT/LOCATION	,	VER WX	FTG
***************************************			496			WX	LEAK RATE TEST-180 SEC		***	
			548	302	10	65 65	1414 SMEAR VS SCAN BOSTON PROVIDENCE	ø'	99 99	
100	Approx		563				HPIVA OPEN			
	and for Re		566	311	3.1 7,9,12	95 95	1414 LENS MTF FLORENCE LINES TUCSON W/5T RESO		99 85	114
	Approved for Release: 2025/07/25 C05127748		629	338	•	75 75	1414 T/F+12,+6,0,-6,0 BOSTON PROVIDENCE		99 99	46
	07/25 CO		631	339	10	75	1414 SMEAR VS SCAN LOS ANGELES		85	88
	15127748		647	346	6.1	95	1414 LENS MTF LUKE LINES		99	52
	, N &		A 1				1208-2 FOOTAGE			702
							ACCUMULATED FOOTAGE			

	3,6	Missio	n 1208-3	Special	Events			
-		REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
		678				TRANSFER TO TU3-PREP 1		
		679				COMPLETE TRANSFER-PREP 2		63
Approved		696	372	12	90	QUALITY VARIABILITY SACRAMENTO/ BAY AREA	80	30
elease:		728	388	6.3	95 95	1414 LENS MTF KINGMAN LINES 1414 LENS MTF QUARTZSITE LINES	99 85	78
!! !! !! !! !! !! !! !!		744	397	7,9,12	90	TUCSON W/5T RESO	99	29
7/25 C05		752				XT-A SET TO +2 STEPS PER PFA DIRECTION	b	
127748		888	456	10	75	1414 SMEAR VS SCAN MONO B@-37° NEW YORK	85	83
		989	491			ESD A/B INDICATION		*
		989 989				MONO A CV MONO B CV		12
		991				MONO A CV VIA DIS		12

	3.6	Mission	1208-3 Sp	eclal	Events-Co	nt'd.	F		· ·
		REV	OPN	TEST	PRE WX	EVENT/LOCATION		VER WX	FTG
		993				SCC 2 SELECT MONO A CV VI A ENA			
Appr		995				SCC HEALTH CHECK VI A DIS			163
oved for		1003	502	6.1	95	1414 LENS MTF FLORENCE LINES		95	50
Release:		1020				MONO A CV VIA ENA/DIS	•		12
2025/		1092				PN EQUALIZE	3		
5/07/25		1099							
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	3.7	Mission	1208-4 S	pecial E	vents			
		REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
		1115				TRANSFER TO TU4-PREP I		i
		1116				COMPLETE TRANSFER-PREP 2		63
		1130					•	
		1811	620	7,9,12	99	TUCSON W/5T RESO	99	29
素		1218	632					
\$3		1268	641			PN EQUALIZE ESD B		
		1277				PN EQUALIZE		
		1279				CREEP B		
		1283				CREEP B	2	*
		1287				DITHER TEST		
		1295				CV A-RELEASED FOR MONO A OPN JOG B	*	64
		1299				CREEP B		7

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		REV	OPN	TEST	PRE WX	EVENT/LOCATION
		1300				SS ENGINEERING RELEASED FOR STEREO OPN
Approved fo		1309	651	3A	75 75	1414 SMEAR SLITS -16,-8 BALTIMORE WASHINGTON
r Rele		1461				PN EQUALIZE
for Release: 2025/07/25 C05127748		1487	719	.3A	65	1414 SMEAR SLITS -16,-8,0 NEW YORK
7/25 C		1501				TRANSFER TO \$0255
05127		1528				PN EQUALIZE
7748		1554	733	4,12	99	SO255 COLOR W/6C LIVERMORE
		1570	741	8	95 95	SO255 COLOR W/6C VAN NUYS SO255 T/F 14,0,-14 LOS ANGELES

4,8

SO255 COLOR W/6C T/F +14 ST LOUIS

Mission 1208-4 Special Events-Cont'd.

3.7

3.7	Mission	1208-4	Special	Events-	Confid.

REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
1596				TRANSFER TO FE3916		
1633	756	30	75	FE3916 SMEAR SLITS PHILADELPHIA	95	31
1635	758	5-	99	FE3916 W/6C STOCKTON	99	29
1651				PN EQUALIZE		
1656				PN EQUALIZE		
1667	764	5	65	FE3916 W/6C TUCSON	95	29
1687				PN EQUALIZE		
1700				PREP 2/CV		DEPLETED
•				1208-4 FOOTAGE		596A 605B
		i.		ACCUMULATED FOOTAGE		2740A 2840B

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3.8

Solo Phase

No solo phase experiments were performed on mission 1208.

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4.0 SENSOR SYSTEM TEST OBJECTIVES

4.1 Photographic Performance

Determine the capability of the SS Optical System to provide the specified photographic performance.

The post flight material evaluation of mission segments 1208-1, 1208-2, 1208-3 and 1208-4 indicated in a general sense the capability of the SS Optical System to provide the specified photographic performance. Mission 1208 was a summer mission launched in April in a non sun synchrous orbit of 94.5° inclination angle, prior to the summer solstice. Summer missions in general acquire a large percentage of photography at solar altitudes above 30 degrees, resulting in smaller operational slits, shorter exposure times and less image smear. The overall image quality, however, was affected to some extent, as it always is at this time of the year, by varying degrees of weather and haze. In addition, specular reflections and shadowless acquisitions resulted in significant image quality degradations to the mission photography, similiar to Mission 1206.

In review, Mission 1206 was launched in July early in the afternoon in a sun synchronous orbit of 96.2 degrees following the summer solstice. This resulted in the specular reflection/front lighting problem to move south in latitude as a function of mission length, and the late launch caused the problem to locate at Nadir and simultaneously affect the imagery from both cameras. The sun synchrous inclination angle caused the problem to remain fixed in scan.

Mission 1208, however, was launched in April, early in the afternoon, prior to the summer solstice, at 94.5° inclination angle, non sun synchronous. This caused the specular reflection/front lighting problem to first move north and then slightly south in latitude. The lower inclination angle increased the precession and moved the local sun time over target closer to morning as the mission progressed. The problem, initially occurring near Nadir, moved across scan, as a function of mission length, ending up at approximately 30-35 degrees of scan at the end of the mission. Thus both cameras did not experience either anomaly at the same scan position.



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A much better operational plan for summer launches would be to launch early in the morning in a sun synchronous orbit. This places the anomaly out in scan, and the sun synchronous orbit fixes its position in scan. This intentional placement of the anomaly out in scan presupposes that operational target acquisition planning will not locate a large percentage of targets at these scan positions. Launching after the summer solstice will move the anomaly south away from the area of interest.

The general overall range in mission image quality for both cameras was very good to poor with the majority rated as fair to good. Orbital performance prediction using CRYSPER and the actual operational parameters are included in Figures 4-1 thru 4-4 for each mission segment and Figure 4-5 for the total mission length. A brief discussion of image quality and general photographic system performance as a function of mission progression is provided, abstracted in part from the PFA Rebound 831 messages.

4.1.1 Mission Segment 1208-1

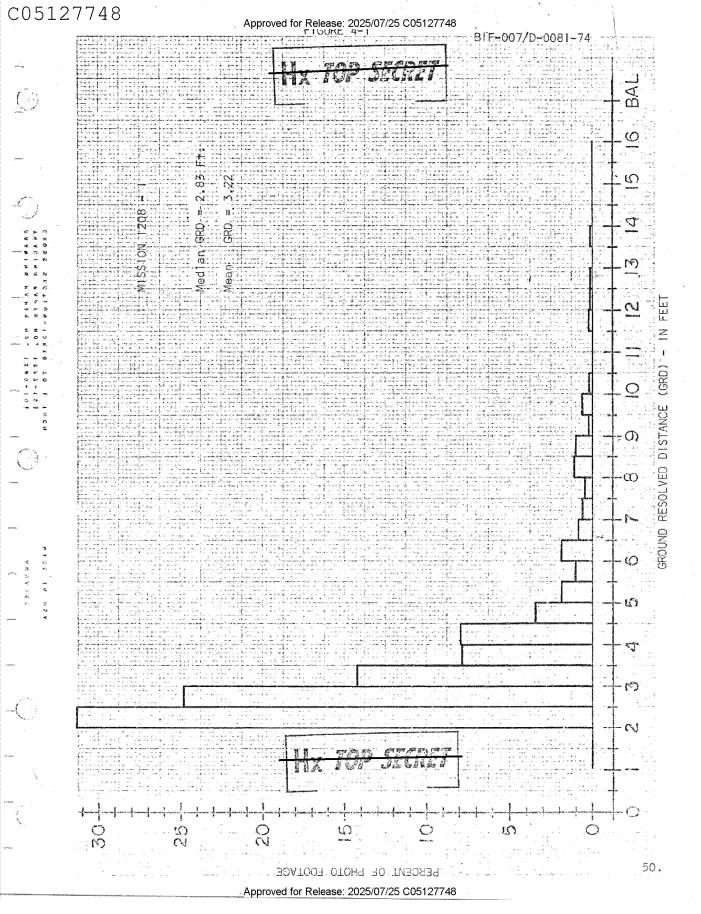
The overall image quality of both cameras ranged from very good to poor with the majority rated as fair. Analysis of the thru focus engineering ops both subjectively and with VEM, resulted in the PFA directing an eight micron retreat to the fwd camera platen, which changed the nominal platen to 76 microns. No focus change was made to the aft camera. In addition to the focus change on the fwd camera, an O2A2 change was required on the aft camera in-track of minus three command steps, resulting in a new in-track nominal setting of minus five command steps. No O2A2 adjustment was made to the fwd camera.

Subjectively, the image quality of the aft camera appeared to be sharper than that of the fwd. In point of fact, the very good imagery on this mission segment, was limited to clear weather acquisitions on the aft camera. The poor image quality which subjectively exhibited an overall grainy appearance, and soft unsharp edges was in part the result of non optimum acquisition conditions, such as high scan angles, cloud cover, medium to heavy haze levels, and the defocused condition of the fwd camera. The very good imagery from the aft camera was comparable to the better photography produced from past Hexagon Missions. This assessment was substantiated by the good resolution readings obtained from the tri-bar corn target, and the direct subjective comparison of image quality from previous Hexagon Missions.

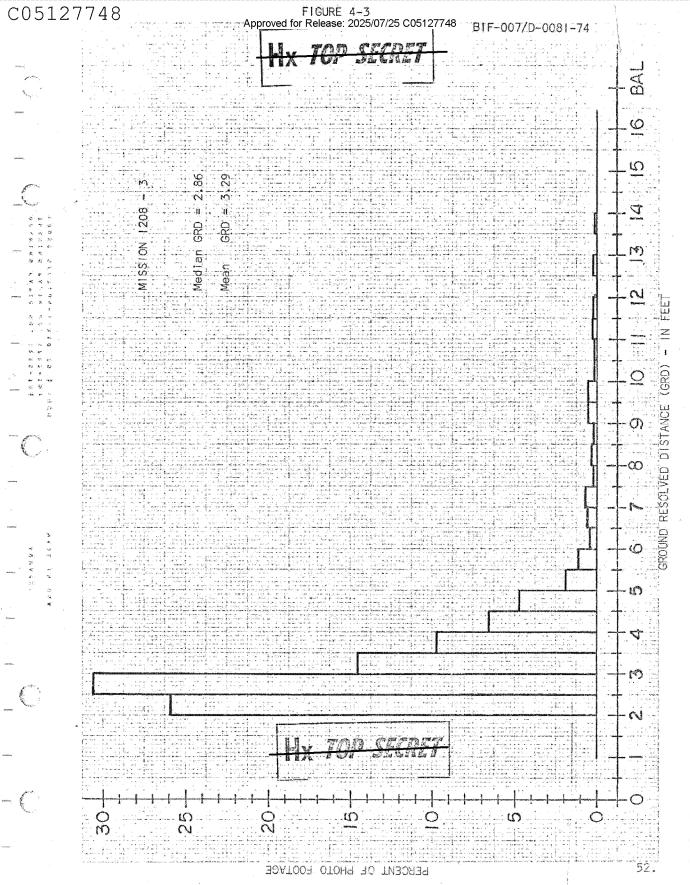
orani'i

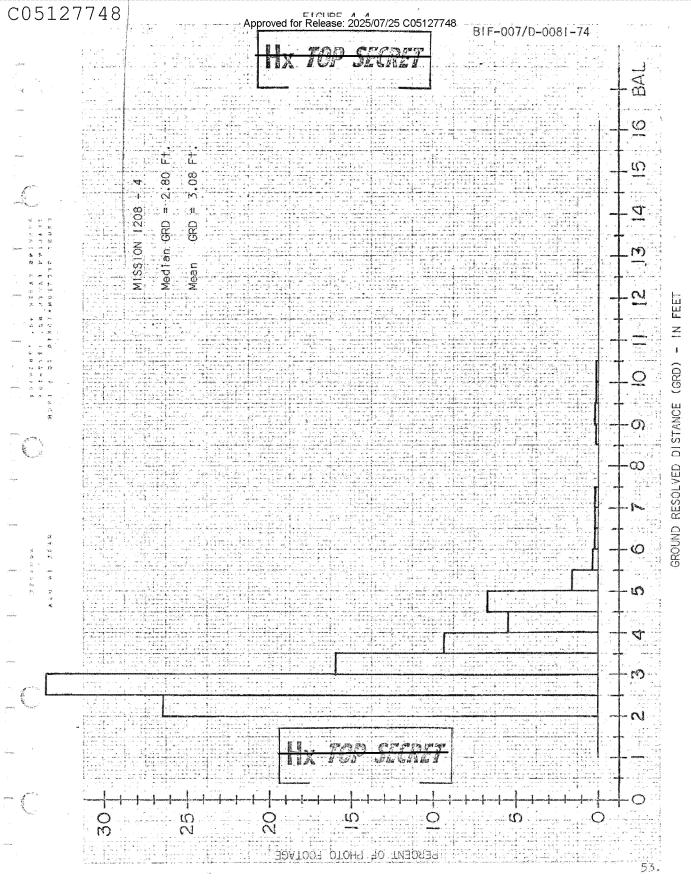
Approved for Release: 2025/07/25 C05127748

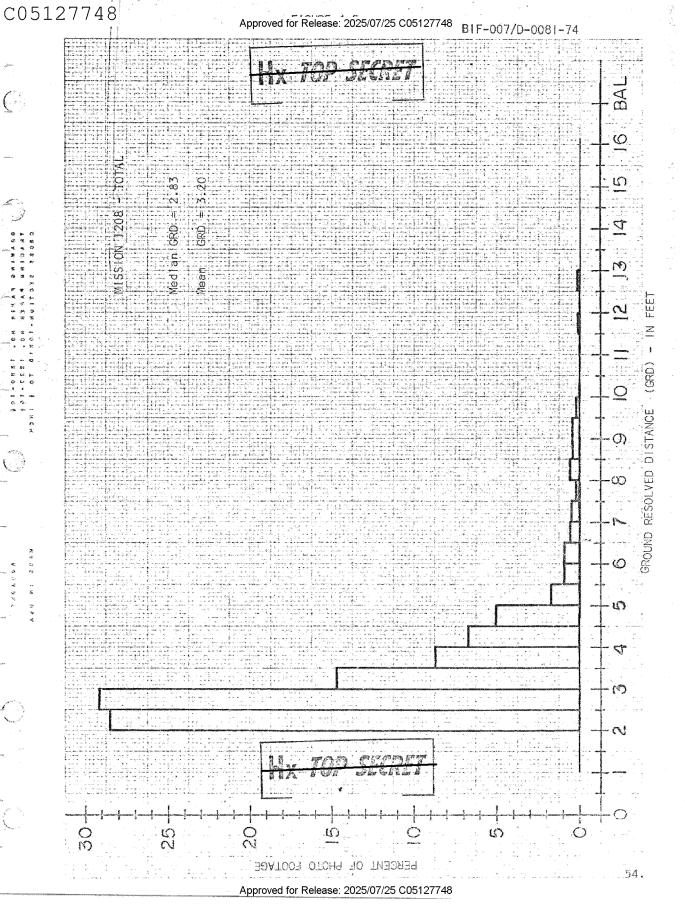
SIRAPA SIRA



51.







One 51/51 tri-bar corn target was acquired on both the fwd and aft cameras. The data follows:

			AN	GLES		UNAI GRD.		2:1 GRD	ADJ (FT)
CAMERA	0P	FRAME	SCAN	FIELD	PLATEN	IT	XT	IT	XT
fwd aft	084 084	004 004	+1.1	-0.8 -2.0	68 25		2.05 2.25	2.06 1.86	2.44 2.73

Exposure on this mission was based on a mean urban/industrial scene density of 1.10 instead of 1.00.

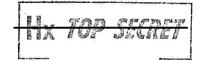
Microdensitometer analysis of 13 frames (9 fwd, 4 aft) with vegetation surround indicated reasonably good exposure (-.02 log E from alm for the fwd, -.05 log E for the aft) requiring no alteration of the 1208 general recommendation. The two count exposure reduction bias given to the aft camera resulted in a better balance exposure between cameras.

The average scene range was found to be higher than was generally recorded for this time of the year. This was true for both foreign and domestic ops. As was generally the case, the scene range of the domestic areas was greater as was the areas acquired by the fwd unit.

Although two snow scenes examined were correctly exposed, portions of two other frames were underexposed (op 58, frame 15 fwd, op 118, frame 17 fwd). In both frames urban areas were grossly underexposed with accompanying low contrast. Evaluation indicated that the snow had melted in the urban areas, and because the urban area represents only a small portion of the frame, the snow bias was correctly applied.

4.1.2 Mission Segment 1208-2

The overall image quality of both cameras improved on 1208-2 from 1208-1. This general improvement was attributed in part to the focus adjustment of plus 8 microns on the fwd camera, and in part to the overall improved atmospherics, resulting from less snow and correspondingly less moisture in the atmosphere. A third contributing factor was the use of the 26DN process employed on 1208-2 because of abnormally high base plus fog on affic sections of both original photographic recor



4.1.2 Mission Segment 1208-2-Contid.

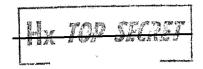
The image quality of both cameras on 1208-2 ranged from very good to poor with the majority rated as fair to good. As with Mission 1208-1, the very good imagery was associated with the aft camera. The aft camera image quality was superior to that of the fwd camera and subjective comparisons very clearly indicate that it was significantly sharper, and the aft camera consistently recorded very fine details. The fwd camera imagery was affected by specular reflections.

One 51/51 tri-bar corn target was acquired on both cameras. The data follows:

		, v	ANGI	LES		UNA GRD	DJ (FT)	2:1 GRD	ADJ (FT)
CAMERA	0P	FR	SCAN	FIELD	·	IT	XT	<u>IT</u>	XT
fwd aft	311 311	12 12	+16 +17	-1.7 -1.5	76 25	1.83	2.38 2.19	2.03 2.05	2.63 2.49

The late launch time of 1208 resulted in specular reflections on the fwd record, and full front lighting (shadowless acquisitions) on the aft photography. This condition occured near Nadir, and between approximately 5 to 30 degrees north latitude on this mission segment. This mission orbit was such that the specular reflections moved out in scan angle as the mission progressed and they were predicted to be at about 35 degrees scan at mission termination. The latitudes affected progressed to the north and then moved slightly south.

Many cases of specular reflections were found in the fwd camera imagery within the latitude bands and scan angles indicated. In this mission segment the effect of the specular reflections appeared more severe than the corresponding shadowless acquisitions. These shadowless acquisitions did in fact produce a loss in contrast due to the reduction of shadows in the scene, and a corresponding reduction in fine detail. The specular reflections occurred where ground water was standing. In these areas there was gross image blooming and loss of localized information in the direct vicinity of these reflections.



4.1.2 Mission Segment 1208-2-Contid.

A high base plus fog condition occurred on approximately 54 percent of the original negative. This condition existed on 1208-1 and was expected to be present throughout the remainder of the mission.

This anomaly was associated with specific manufactured film rolls and the probable cause was a pelloid backing contaminant, which, when in contact with the emulsion, caused a fog build-up with time, reduction of the density range, and a small speed and contrast change.

In an effort to compensate for the sensitometric change induced by the high fog found on 1208-1, EK evaluated several modified 19 DN processes. One of these, designated 26 DN, was selected for use on those segments of 1208-2 that could be expected to exhibit high fog in the standard 19 DN process. The 26 DN process reduced the fog somewhat and retained the desired sensitometry. Flashed stock was inserted at those manufacturing splices where a change from 19 DN to 26 DN or vise versa was required.

The developer switch was then accomplished as these flashed stock inserts were being processed and imagery was not affected by the transitions.

Comparisons were made of the duplicate positives from the normally processed low fog film, the 26 DN processed fogged film, and normally processed fogged film from 1208-1. The slightly increased contrast and the lower fog density of the 26 DN processed film over the 1208-1 fogged film was evident. More shadow and highlight detail was present in the imagery. Little discernable difference in image quality was present in comparisons made between the 26 DN processed fogged film and the normally processed low fog film in 1208-2.

Microdensitometer analysis of 29 acquisitions of vegetation surround, urban/industrial area imagery indicated generally satisfactory exposure with either 19 DN or 26 DN processing. The 26 DN process demonstrated higher contrast of the scene imagery accompanied by a slighter higher exposure of the scene mean (.02 log E). The high base fog level did not adversely affect any vegatation surround scene examined.



4.1.2 Mission Segment 1208-2-Cont'd.

Continued monitoring of springtime snow surround imagery indicated increased occurance of underexposed and flat imagery of cultured areas due to melted and/or dirty snow within the area of interest. Examples of this appeared in ops 307 and 308 where underexposure ranged up to a stop.

Because of the magnitude and frequency of underexposure of snow surround scenes, the following snow bias criteria was recommended for the remainder of the mission:

Reported Snow Depth

Exposure Blas

Less than 2 inches 2 to 10 inches

No bias
-.13 log E

Greater than 10 inches

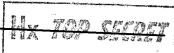
-.26 log E

While this change did not totally optimize exposure of snow surround scenes it was designed to prevent complete loss of information in shadow areas without grossly overexposing areas of existing snow.

4.1.3 Mission Segment 1208-3

The overall image quality of both cameras ranged from poor to very good. This imagery was comparable to 1208-2. The instances of poor photography was attributed to atmospheric conditions, very high sun angles, specular reflections, and shadowless imagery. The aft camera image quality was superior to that of the forward and most of the very good imagery was on the aft record. The presence of specular reflections and shadowless acquisitions, particularly front lighting, continued to significantly degrade a large portion of the photography from this mission.

These problems, particularly that of the front lighting, became more severe during this mission segment, with approximately 40 percent of the frames affected by front lighting. The most severe front lighting was similar to that seen on 1206. The problem was primarily due to the present sun/orbit geometry and large number of acquisitions in the latitude range from approximately 10 to 50 degrees north. Objects acquired between minus 10 and minus 20 degrees scan at these latitudes were degraded by front lighting, and objects acquired between plus 10 and plus 20 degrees were affected by specular reflections.



4.1.3 Mission Segment 1208-3-Cont'd.

For acquisitions within this latitude range north of the sub-solar point the aft camera was affected by front lighting, and the fwd camera experienced specular reflections. The effects appeared on opposite cameras in acquisitions south of the sub-solar point.

The magnitude of the degradation resulting from front lighting was dependent upon the camera to target to sun acquisition angle (cats angle). The extent of area affected ranged from a few degrees to as much as 20 degrees of scan in the most severe cases. The image degradation from the front lighting was more extensive than that from the specular reflections. All targets acquired with front lighting exhibited some degree of degradation, whereas specular reflections tended to degrade only high reflectance objects and their surroundings.

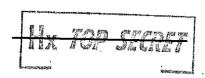
One 51/51 tri-bar corn target was acquired on both the fwd and aft cameras. The data follows:

						UNA			ADJ
			AN	IGLES		GRD.	(FT)	GRD.	(FT)
CAMERA	OP	FRAME	SCAN	FIELD	PLATEN	IT	XT	IT	XT
fwd	397	3	-	-1.5	76	1.7	2.5	1.9	2.8
aft	397	3	-	-1.3	. 25	1.2	2.1	1.4	2.3

Microdensitometer analysis of vegetation surround urban area imagery indicated continued good exposure. There was also no significant change in mean scene density between use of 19 DN and 26 DN process chemistry. The following table gives the average exposure error of all vegetation surround scenes analyzed on 1208 (approx. 35 scenes) based on the optimum exposure criteria of 1.1 density.

AVG. MEASURED LOG EXPOSURE ERROR

		19 DN	26 DN
camera camera	×	minus .02 minus .04	minus .03 minus .04



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4.1.4 Mission Segment 1208-4

This mission segment contained 2588 feet of SO-255 conventional color material, and 3036 feet of FE-3916 infrared color material in addition to the regular 1414 black and white material. The photographic performance for each material type is as follows:

Film Type 1414 - Black and White
The overall image quality of 1208-4 ranged from good
to poor with the majority rated as fair to good. The
instances of poor photography again were attributed in
part to localized atmospheric conditions and specular/
shadowless acquisitions. As with earlier mission
segments the majority of the good imagery was associated
with the aft camera. The aft camera image quality was
superior to that of the fwd in that it was sharper.
The combination of haze and shadowless acquisitions
resulted in poor imagery which can be characterized as
flat and grainy. This yielded imagery with soft and
unsharp edges and significant loss in fine detail.
This condition had a lesser impact on total performance
than on 1208-3.

Five 51/51 tri-bar corn targets were acquired on the fwd camera and one target on the aft camera. The data follows:

			ANG	LES		UNAI GRD.		2:1 / GRD.	
CAMERA	OP	FRAME	SCAN	FIELD	PLATEN	JT	XT	ΙT	XT
fwd aft fwd fwd fwd fwd	620 620 741 745 758 764	3 4 4 3 3	+21.0 +22.0 -16.0 - 8.0 -27.5 +14.0	+1.9 +0.1 -0.3 -2.3 -2.5	76 25 76 76 76	2.10 1.72 1.85 2.20	3.27 2.67 1.95 2.25 3.04 2.66	2.10 2.58 2.24 3.25	3.99 2.68 2.89 2.80 4.37 2.80

Film Type \$0-255 - Conventional Color

The quality of the imagery (for color film) ranged from very good to poor, with mos rated good. The very good imagery was comparable to the duality SO-255 acquired with the Hexagon System to date (1). Poor imagery was generally associated with large ants of haze. The color balance of the original was startly yellow-green, and was similar to that of the SO-255 acquired on Mission 1207-1. Subjective evaluation of engineering photography for focus evaluation showed the nominal focus setting to be acceptable, although a slight bias to the plus side(6 microns) might have been in order.

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4.1.4 Mission Segment 1208-4-Cont'd.

Subjective evaluation of exposure showed the original to be slightly overexposed.

Two 51/51 corn tri-bar targets were acquired on SO-255 film. The data follows:

			ANGI	_ES		GRD.	(FT)
CAMERA	OP	FRAME	SCAN	FIELD	PLATEN	IT	XT
af†	741	4	-15.3	-2.3	55	2.83	3.03
af†	745	3	- 8.0	-0.5	55	3.17	4.03

NOTE: Procedures for the 2:1 contrast adjustment have not been established for SO-255.

Film Type FE-3916 - (Infrared color)

The overall image quality of the FE-3916 material was good, and was comparable to that of 1207-4. The fine detail quality of the 3916, however, continues to be significantly less than that of the conventional black and white 1414 material utilized on the fwd camera. The color balance of the original has a slight cyan cast; subjective evaluation of the photography showed the exposure to be adequate.

Two 51/51 tri-bar corn targets were acquired on the aft camera on the FE-3916 material. The data follows:

			ANGL	ES		UNA GRD.	DJ (FT)
CAMERA	OP	FRAME	SCAN	FIELD	PLATEN	IT	XT
aft aft	758 764	3 4	-27.5 +15.0	-2.5 -2.3	55 55	5.66 4.80	6.21 5.94

NOTE: Procedures for the 2:1 contrast adjustment have not been established for FE-3916.

The presence of specular reflections and shadowless acquisitions, particularly front lighting, continued to degrade portions of the photography from this mission segment.

The extent of the degradation within a frame (slight to severe) was approximately plus and minus 10 degrees of scan about the minimum cats angle with the most severe cases occurring between minus 20 and minus 30 degrees of scan at a latitude range of 40 to 45 degrees north for this mission segment.

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4.1.4 Mission Segment 1208-4-Cont'd.

Microdensitometer analysis of six SO-255 urban area acquisitions indicated an overexposure of approximately 0.10 log E. This overexposure was due in part to the overall scene brightness increase inherent in low shadow acquisitions. Low shadow scenes appeared quite frequently in aft camera acquisitions. This condition also appeared regularly in Mission 1206 with the same results in exposure. This amount of overexposure was considered significant and may have to be considered in the predictions of future summer missions.

Evaluation of three FE-3916 acquisitions showed a 0.08 log E overexposure. This was probably due in part to the shadowless conditions as well.

Although no microsensitometry was done on 1414 film in 1208-4 observation of clear weather imagery subjectively indicated continuing good exposure.

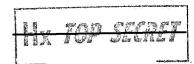
4.2 Take-Up Survival Thru Recovery

All the RV/TU assemblies arrived at the BRIDGEHEAD processing facility in good condition, with 1208-1 being a water recovery, and 1208-2,3 and 4 conventional air recoveries. The ability to maintain light tight integrity during orbital operations, separation, re-entry, recovery and transportation to the processing site, was fully demonstrated. The core locking pins were engaged and intact in TU's 1208-1,2 and 4 with the film well centered and stacked. The fwd camera core locking pin of TU 1208-3 was engaged and sheared and approximately 50 feet of film was spilled; on the aft camera, the core locking pin was engaged and bent causing some damage to the RV during pin removal. The film was well centered and stacked on both TU's of 1208-3. Small amounts of particulates were found in all the RV canisters.

Related de-filming observations for each mission segment follows:

4.2.1 Mission Segment 1208-1

The RV/TU arrived at the processing facility in good condition. All parachute apparatus was wet. The RV cover recesses had small amounts of water in them resulting from the wet recovery. The battery discharge units had not been installed on the RV. Both core locking pins were engaged and intact.



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4.2.1 Mission Segment 1208-1-Conttd.

Both film rolls were dry, well stacked and well centered in the T/U. A small amount of particulate was collected from the inside of the dome, as well as a one-inch long piece of wire which had been lodged in the fwd roll at OP 038 and had punctured four convolutions of the film. A severe dimple was detected near the head of the fwd roll at presplice. The cause was not found, but correlated with the puncture of fwd OP 001 IOR. Tag ends were removed and processed prior to normal defilming to allow early PFA team image quality evaluation.

4.2.2 Mission Segment 1208-2

The RV/TU arrived at the processing facility in good condition. Both core locking pins were engaged and intact. Both rolls were well stacked and well centered on the TU with no festooning into the dome. The hinge and thermal access door on the entrance side was sprung. A white residue was noted around the fwd side exit door and cutter assembly.

During despooling it was discovered that the brake on the fwd side was not operational. It was commanded "on" several times but no braking could be accomplished. The audible sound of the brake solenoid actuation was detected thus concluding the problem to be in the brake assembly. This necessitated hand held tension on the stack when the motor was turned off for splicing.

Two deep scratches were noted inside the dome and a I inch tear in the acrylic tape covering the fiberglass on the relay housing was noted on the fwd side adjacent to a canister alighment pin.

The dome was clean with only a small amount of particulate retrieved.

4.2.3 Mission Segment 1208-3

The RV/TU arrived at the processing facility in good condition.

Upon removal of the RV canister, it was evident that the de-orbit core locking pin on the fwd side had sheared resulting in a 50 foot film spill. Prior to handling the film, the builder roller arms were raised



63.

4.2.3 Mission Segment 1208-3-Cont'd.

electrically using special test equipment. This was to preclude possible damage to the builder roller verify microswitch on the fwd side which evidenced intermittent failure during the mission. The 50 feet of spilled film was then responded onto the TU stack.

The film stacks were good with the exception of a rough edge on the inside of the fwd stack approximately 3/4 inch from the outside diameter.

The most significant problem occurred when attempting to withdraw the aft core locking pin that had been bent during recovery. Normal techniques for removing a bent pin failed, requiring the pin assembly to be drilled out. This effort consumed 18 hours. However, processing time was not lost because the fwd side film was processed in parallel with this effort.

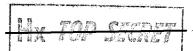
The RV suffered the following damage during removal of the bent core locking pin:

- 1. Complete destruction of the piston and actuating pin.
- 2. Cut wire bundle and damage to the solenoid assembly.
- 3. Removal and damage to actuator assembly plate.
- 4. A fracture in the support assembly cross frame member of approximately 7mm.
- 5. Damage to primary battery.
- 6. Minor physical damage (rubs, abrasions, etc.) to the aft side wire bundles in area of A-2 canister recess.

A small amount of particulate was retrieved from the dome.

4.2.4 Mission Segment 1208-4

The RV/TU arrived at the processing facility in good condition. No major problems occurred. The film stacks were good and the de-orbit pins did not shear. A small amount of shredded film was found in the RV cannister. The film was damaged by pulling the loose ends thru the camera. The TU electronics (A-2 and A-15) on aff side were removed and sent directly to the vendor for analysis of the integrator reset problem experienced during 1208-4 mission segment.



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4.3 Optimum Focus Determination

Mission 1208 (SV8/SNII) was launched with orbital focal plane settings of 68 microns on the forward camera and 25 microns on the aft camera. These settings included a plus 14 micron adjustment on both cameras for the altitude shift from infinity (A-2 collimator settings) to 85 nautical miles mission altitude. They also included a minus 15 micron adjustment on the forward camera and a minus 19 microns on the aft camera for the folding flat gravity effects. The forward camera was further adjusted plus 2 microns to account for a defocus of the test collimator.

Following the evaluation of the on orbit thru-focus tests in RV-1 a retreat of plus 8 microns was recommended for the forward camera. The forward platen was retreated to 76 microns on OP 156. No focus change was deemed necessary for the aft camera.

A change in focus of plus 30 microns retreat was implemented on the aft camera when the material switched from 1414 black and white to the SO-255 conventional color. This focal plane position was also utilized for the FE-3916 infrared color material.

4.4 Optimum OOAA Settings

On-Orbit smear data was collected during all four of the mission segments of Mission 1208, on either the 1414 material or on the FE-3916 infrared color. No smear data was collected on the SO-255 conventional color material.

Analysis of the smear test material from mission segment 1208-1 identified an aft camera in-track velocity error. It was determined that the film velocity was 0.023 ips too fast and the PFA directed a minus three command step change to correct it. The ground settings for the forward camera, in-track and cross-track and the aft camera cross-track were determined to be correct. It is interesting to note that since the first use of smear slits on SV-6, all three systems have required an identical change to the aft camera in-track settings. This phenomenon is currently under investigation.

On mission segment 1208-2 ninety data points were measured from each camera. The minus three command step change made to the aft camera in the in-track direction was verified to be correct and within less than one command step of the indicated



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4.4 Optimum OOAA Settings-Cont'd.

zero setting. The forward camera in the cross-track direction showed that the indicated mean error was slightly greater than one command step and was changed accordingly by plus one command step. The forward camera in-track and aft camera cross-track directions were both confirmed to be properly set. The smear slit imagery, both subjectively and objectively, indicated higher smear variability then past systems. Only one smear test (a type 10) was run on mission segment 1208-3, and this was a mono run on the aft camera. This data was not reduced.

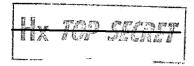
Mission segment 1208-4 contained 2588 feet of SO-255 color and 3036 feet of FE-3916 infrared color material included in the aft camera record. No OOAA tests were acquired on the SO-255 material, however, subjective evaluation of the smear slit imagery indicated that the cross-track bias was adequate to account for the difference in material thickness.

A subjective evaluation of the smear slit imagery acquired on the FE-3916 material was performed. The inherent low resolution level of the 1R film and subsequent very poor image quality in the smear slits negated any quantitave measurement or subjective assessment of the cross-track film synchronization. The PFA recommended that this test on FE-3916 not be performed on subsequent missions. Special thru-focus/ 0^2 A2 bias tests were conducted during this mission segment to determine if the minus eight microns focal plane bias was optimum. Analysis of the material indicated that the bias magnitude and direction was necessary and adequate.

4.5 Optics Thermal Profile

The following subparagraphs describe the thermal environment for Mission 1208. Definitions of measured and calculated temperature parameters are contained in the Mission 1207 Post Flight Report, PM-1496-X. Thermal control for SV-8 can be generally summarized as follows:

 All SS temperatures were within design limits throughout the mission.



4.5.1 SV Environment

SV thermal control parameters are summarized as follows:

Orbital Elements (Ref. Paragraph 1.5)

Perigee Altitude

 $h_{p} = 85.6 \text{ n.m.}$

Period

 $\tau = 88.5 \text{ min.}$

Inclination

 $I = 94.5 \deg.$

Argument of Perigee

 $\alpha = 130$ deg.

Beta

 $\beta = -2.6 \text{ deg. (Rev I)}$ $\beta = 26.5 \text{ deg. (Rev I692)}$

Midsection Thermal Control Design Values

Cocoon

 $\alpha/\epsilon = 0.359/0.265$

Thermal Baffle

 $\alpha/\epsilon = 0.90/0.90$

MLI Effective Emittance

Lower 210 Degrees

e* = 0.0045

Fwd & Aft Bulkheads

 $\epsilon * = 0.0045$

Viewport Baffle

 $\epsilon * = 0.0045$

Under TCA Cocoon

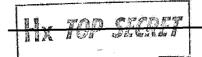
 $\varepsilon * = 0.04$

Under SU Cocoon

 $\epsilon^* = 0.6$

4.5.2 TCA Environment

Table 4 - I is a summary of temperature levels, spatial distributions, and temporal variations over a typical orbital revolution in terms of the thermal ICD (1420316A) requirements. Figures 4-6 thru 4-8 show the corresponding orbital profiles of the ICD parameters.

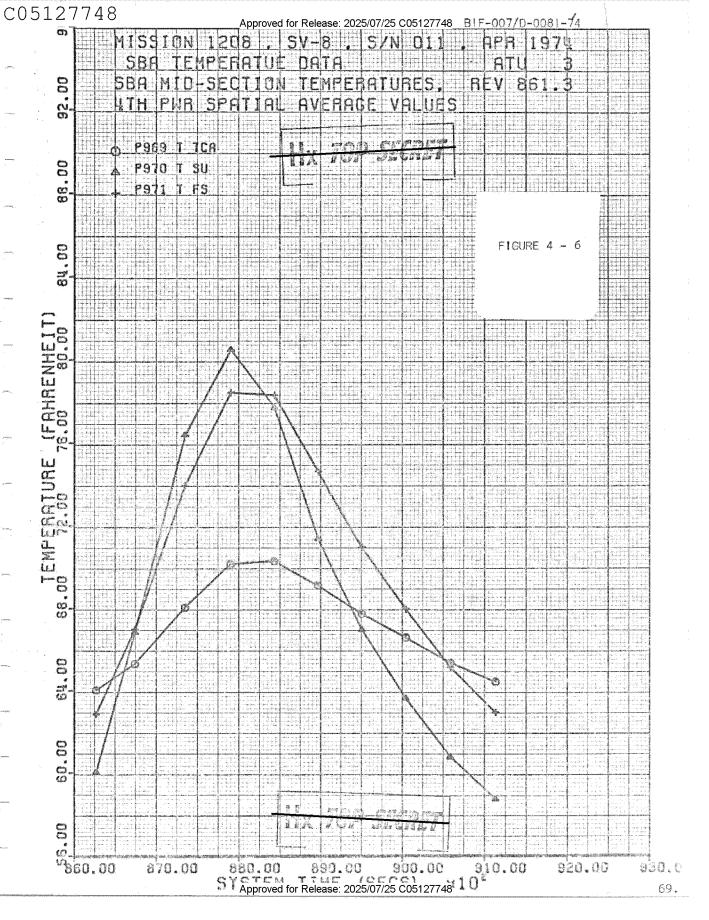


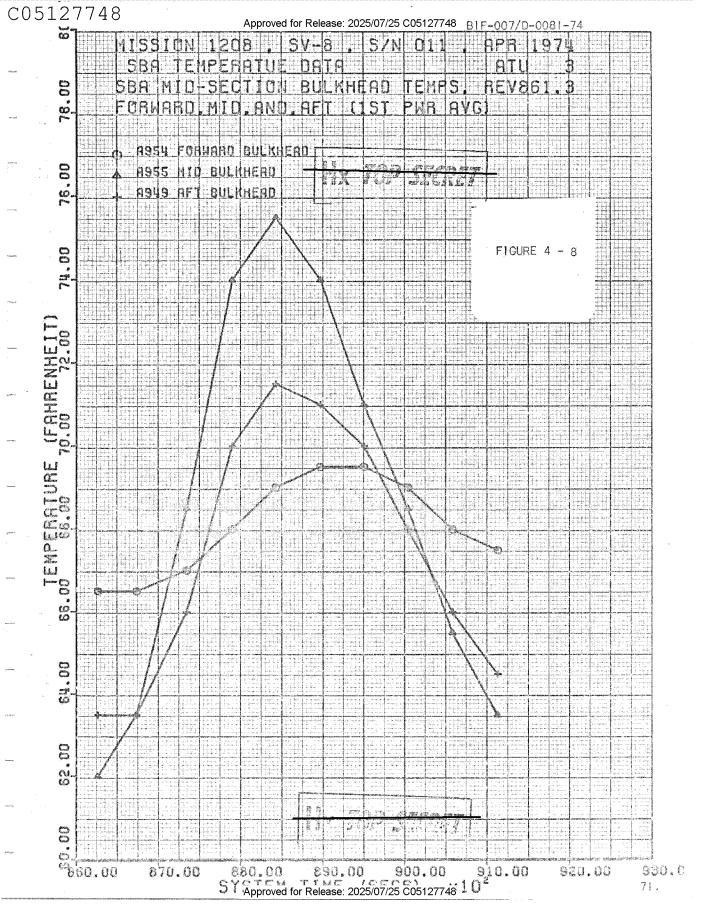
TCA COMPARTMENT TEMPERATURES

(MISSION 1208 REV 861)

- E (10n)	Designated Zones	Max Allowable ICD Value(°f)	Flight Value(°f)
Temperature Level Index (T TCA) Zone I Mean Temp. Zone II Mean Temp. Zone III Mean Temp. Zone IV Mean Temp. Forward Bulkhead Middle Bulkhead	Not Applicable	70 ± 21 N/A N/A N/A N/A N/A N/A	67 67 65 66 69 68 69
Variation of Mean Temp. Between Designated Zones	l to IV II to III I to IV Bulkhead to Bulkhead	9 6 4 4 6	2 2 3
Spatial Variation of Time-Average Temp. Measurements at Locations Within Designated Zone	l V Forward Bulkhead Middle Bulkhead	11 9 9 11 5 17	5 2 I I 2 6
Temporal Variation (Peak to Valley) of Temperature Measurement at any one Location within Designated Zone	 	46 20 20 46 26 57	17 1 1 17 4 16

Approved for Release: 2025/07/25 C05127748



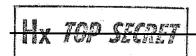


C05127748



4.5.3 Optical Bar Temperatures

Tref was 67 $^{\pm}$ 1°f throughout the mission. The equilibrium temperature levels for the A and B optical bars were approximately 66°f and 65°f respectively. Figure 4 - 9 shows an orbital profile of the OB temperatures in the stowed position.



73.

5.0 SCF SUPPORT

5.1 'TUNITY 'Mission 1208

The 'TUNITY MOD-2 software for Mission 1208 performed all of its functions nominally except for the following software problems.

In message 350, Rev 123, Operation 3, a desert polygon bias was applied where no desert polygon had been defined. This caused the operation to be under-exposed. A change was made to 'TAPWRP correcting the problem. The change was incorporated on the Flight Auxiliary Master.

Check message 38 appeared often, flagging insufficient time between FT- and C-. Errors flagged ranged up to .289 seconds. This problem occurred by tightening check message 38. The problem was determined to be flight critical because message 38 was in error due to truncation in both 'TFUNCHK and 'TUMP. Changes were made to both 'TFUNCHK and 'TUMP correcting the problem. The change was incorporated on the Flight Auxiliary Master.

5.2 Augie

5.2.1 Overall Performance

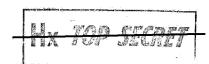
Real time performance of Augie data met all requirements expected. SSC real time modes are limited to verification of SS status. Playback performance of Augie data met all requirements expected. Time delays for play backs of data was reasonable with few exceptions.

5.2.2 Modifications

No changes to the Augie modes were required during the flight. One MCR was required to correct the processing of the shutter open and close telemetry monitors, this was a deficiency in the handling of the data by the mode processing.

Mode Change Requests have been submitted to change or add telemetry data processing to the mode for the next flight. The MCR's submitted are for the following reasons:

a. Change processing of shutter open and close telemetry so as to calculate and output shutter open and close times to OB position in degrees.



5.2.2 Modifications-Cont'd.

- Correct Supply Command Signal processing to increase accuracy of output.
- Output slit width A & B telemetry data by using the change in DIU counter to clock out the next sample of slit width A & B telemetry data.
- d. Add Take-up Integrator Output telemetry monitors to the Format C diagnostic modes.

5.2.3 D.T.V.

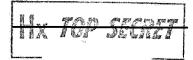
SSC utilization of the DTV was limited to passive real time SS status verification. The use of the DTV will remain limited to status monitoring on the next flight also.

5.3 RTS Tapes and Microwave

5.3.1 RTS Tapes

RTS tapes were used minimally during the last half of the flight due to use of the microwave link between the STC and Bldg. 156. The tapes that were utilized, the majority being COOK, met SSC requirements with few exceptions.

5.3.2 The microwave capability between the STC and Bldg. 156 did reduce the number of tapes required by SSC tremendously. The link did experience many problems during the first portion of the flight, most of the problems fell into the category of not having the proper procedures set-up, however, most of these problems were corrected during the flight. Continued use of the microwave link with the STC is planned for the next flight.

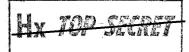


Hx TOP SECRET

APPENDIX

A-1

OPERATIONAL SUMMARY



CAMERA OPERATIONS SUMMARY REVS PAD THROUGH REV 225, OP 131

ŧΕV	MSN CP	SCA	SCC	FRAI	4ES	INT	ERCP	PHOT	C-FT	CUM-TU	-FEET
poder	NUM			FhC	AFT	FWC	AFT	CWD	AFT	és n	8 C T
RE	LC	6:C	0	F N C		7.2	78	FWD		FND	AFT
PRE			0		6			33	3.3	105	111
	LC	60	0	6	6.	35	34	33	3.3	173	178
-⊅8E	LO.	3 C	30	6	6	76	69	17	17	266	264
RE.	FC	6 C	25	7	4	11	2.0	40	2.3	317	307
PRE	LO	30	30	6	6	3	11	17	17	337	335
PRE	LC	60	15	7	4	11	20	40	23	388	378
*RE	LC	12C	C	8.	8	38	7. C	87	87	513	535
₽RE	ĻC	120	C	8	8	111	111	87	87	711	733
PRE	LC	6 C	0.	ć	6	81	65	33	3.3	825	831
⇒RE	LC	6 C	Q:	6	6	31	31	33	33	889	895
≥R E	LO	60	C	6	6	31	31	33	33	953	959
PRE	1.0	3 C	3.0	ć	6	68	53	1.7	17	1038	1029
~⊅RE	LC	6 C	15	7	4	1.1	20	40	23	1089	1072
PRE	LG	6.C	C	6	6	8	163	33	33	1130	1268
PRE	rc	3.0	30	6	6	26	18	17	17	1173	1303
PRE	LO	60	15	7	4	11	20	40	23	1224	1346
⇒8E	La	120	Ĉ	8	8	38	7 C	87	87	1349	1503
2RE	L C	120	Ö	8		111	111	87	87	1547	1761
					8						
PRE	LO	6 C	Č	6.	6	81	65	33	33	1661	1799
TORE	LO	60	0	6	6	31	3 <u>1</u>	33	33	1725	1863
PRE	LC	6 C	G	6	6	31	31	33	3.3	1789	1927
PRE	LC	6 C	C	6	6	31	31	33	3.3	1853	1991
- 4	3.	60	0	6	6.	126	126	33	33	2C12	215C
4	2	6.C	-15	6	6	24	25	33	33	2069	2208
4	3	6 C	3 C	6	6	36	35	33	3 3	2138	2276
5	4	30	-30	50	50	3.0	24	145	145	2313	2445
6	5	6 C	O.	31	31	22	30	171	171	25C6	2646
7	6	90	Ü	3.8	38	4.8	55	308	3 C 8	2862	3009
7	7	3 C	0	7	7	49	23	20	2.0	2931	3062
8	8	6.0	e	6.	6.	19	28	33	3.3	2993	2123
8	9	6 C	3.0	16	16	36	34	8.8	8.8	31.07	3245
g	10	6 C	-15	16	16	35	37	9.8	88	3230	337C
- 10	11	90	C	6.8	68	4.6	5.3	551	55X	3827	3974
10	12	90	Q.	23	23	67	6.7	186	186	4080	4227
14	23	3 C	õ	14	14	49	33	40	4 C	4169	4300
16	14	3.0	ā	5	5	14	14	14	15	4197	4329
19	15	3.0	3.0	7	7	14	13	20	2.0	4231	4362
21		3 C	-45	53	53	14	14		148	4393	4524
	16							148			
21	1.7	60	1.5	23	23	22	29	127	127	4541	4680
23	1.8	90	0	25	25	50.	57	203	203	4754	4940
24	15	6.0	-30	23	2.3	5.5	4.8	127	127	4976	5115
25	20	3 C	-30	1.0	10	28	20	28	28	5032	51.63
- 25	21	6 C	-15	8	8	20	28	44	44	5 C S 6	5235

25 22 9C C 68 68 46 53 25 23 90 15 15 15 67 66 26 24 9C O 28 28 67 67 26 25 6C O 5C 5C 55 48 26 26 3C 3C 28 28 29 22 27 27 3C 45 25 25 14 14 28 28 3C 45 16 16 13 13 38 29 12C O 62 62 36 7C 38 3C 6C -3C 36 36 79 64 38 31 6C 15 13 13 37 36 39 32 9C 15 22 22 44 51 41 34 9C O 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 3C 28 28 3C 22 42 37 6C 15 19 19 21 29 43 38 6C -3C 26 26 34 36	551 551 5693 5839 122 122 5882 6027 227 227 6176 6321 275 275 6506 6644 81 81 6616 6747 73 73 6703 6834 46 46 6762 6893 664 664 7462 7627 198 198 7739 7889 72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
26 24 9C 0 28 28 67 67 26 25 6C 0 5C 5C 5C 55 48 26 26 26 3C 3C 3C 28 28 29 22 27 27 3C 45 25 25 14 14 24 28 28 3C 45 16 16 13 13 38 29 12C 0 62 62 36 7C 38 3C 6C -3C 36 36 79 64 38 3C 6C -15 13 13 37 36 39 32 9C 15 22 22 44 51 41 34 9C 0 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 3C 3C 28 28 3C 22 42 37 6C 15 19 19 21 29 743 38 6C -3C 26 26 34 36	122 122 5882 6027 227 227 6176 6321 275 275 6506 6644 81 81 6616 6747 73 73 6703 6834 46 46 6762 6893 664 664 7462 7627 198 198 7739 7889 72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
26 24 9C 0 28 28 67 67 26 25 6C 0 5C 5C 5C 55 48 26 26 26 3C 3C 3C 28 28 29 22 27 27 3C 45 25 25 14 14 24 28 28 3C 45 16 16 13 13 38 29 12C 0 62 62 36 7C 38 3C 6C -3C 36 36 79 64 38 3C 6C -15 13 13 37 36 39 32 9C 15 22 22 44 51 41 34 9C 0 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 3C 3C 28 28 3C 22 42 37 6C 15 19 19 21 29 743 38 6C -3C 26 26 34 36	227 227 6176 6321 275 275 6506 6644 81 81 6616 6747 73 73 6703 6834 46 46 6762 6893 664 664 7462 7627 198 198 7739 7889 72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
26 25 6C 0 5C 50 55 48 26 26 3C 3O 28 28 29 22 27 27 3C 45 25 25 14 14 28 28 3C 45 16 16 13 13 38 29 12C 0 62 62 36 70 38 3C 6C -3O 36 36 79 64 -38 3L 6C .15 L3 L3 37 36 39 32 9C 15 22 22 24 51 4L 33 6C -3C 35 35 52 46 4L 34 9C 0 108 108 5C 57 4L 35 6C 15 18 18 57 49 4L 36 3C 3O 28 28 3C 22 42 37 6C 1	275 275 6506 6644 81 81 6616 6747 73 73 6703 6834 46 46 6762 6893 664 664 7462 7627 198 198 7739 7889 72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
26 26 3C 3C 28 28 29 22 27 27 3C 45 25 25 14 14 14 -28 28 3C 45 16 16 13 13 38 29 12C C 62 62 36 7C 38 3C 6C -3C 36 36 36 79 64 -38 31 6C .15 13 13 37 36 39 32 9C 15 22 22 44 51 41 33 6C -3C 35 35 52 46 41 34 9C C 168 108 5C 57 41 35 6C 15 18 18 18 57 49 41 36 3C 3C 28 28 3C 22 42 37 6C 15 19 19 21 29 743 38 6C -3C 26 26 34 36	81 81 6616 6747 73 73 6703 6834 46 46 6762 6893 664 664 7462 7627 198 198 7739 7889 72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
27 27 3C 45 25 25 14 14 14 -28 28 3C 45 16 16 13 13 38 29 12C 0 62 62 36 70 38 3C 6C -30 36 36 79 64 -38 31 6C .15 13 13 37 36 39 32 9C 15 22 22 44 51 41 33 6C -3C 35 35 52 46 41 34 9C 0 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 30 28 28 3C 22 42 37 6C 15 19 19 21 29 743 38 6C +30 26 26 34 36	73 73 6703 6834 46 46 6762 6893 664 664 7462 7627 198 198 7739 7889 72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
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38 29 12C 0 62 62 36 70 38 3C 6C -30 36 36 79 64 -38 31 6C 15 13 13 37 36 39 32 9C 15 22 22 44 51 41 33 6C -3C 35 35 52 46 41 34 9C 0 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 30 28 28 3C 22 42 37 6C 15 19 19 21 29 643 38 6C -30 26 26 34 36	664 664 7462 7627 198 198 7739 7889 72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
38 3C 6C -30 36 36 79 64 -38 31 6C 15 13 13 37 36 39 32 9C 15 22 22 44 51 41 33 6C -3C 35 35 52 46 41 34 9C 0 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 30 28 28 3C 22 42 37 6C 15 19 19 21 29 -43 38 6C -30 26 26 34 36	198 198 7739 7889 72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
- 38 31 6C 15 13 13 37 36 39 32 9C 15 22 22 44 51 41 33 6C -3C 35 35 52 46 41 34 9C 0 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 3C 28 28 3C 22 42 37 6C 15 19 19 21 29 743 38 6C -3O 26 26 34 36	72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
- 38 31 6C 15 13 13 37 36 39 32 9C 15 22 22 44 51 41 33 6C -3C 35 35 52 46 41 34 9C 0 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 3C 28 28 3C 22 42 37 6C 15 19 19 21 29 743 38 6C -3O 26 26 34 36	72 72 7848 7997 178 178 8070 8226 193 193 8315 8465 875 875 9240 9397 99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
39 32 9C 15 22 22 44 51 41 33 6C -3C 35 35 52 46 41 34 9C 0 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 3C 28 28 3C 22 42 37 6C 15 19 19 21 29 743 38 6C -3O 26 26 34 36	178 178 807C 8226 193 193 8315 8465 875 875 924C 9397 99 99 9396 9545 81 81 95C7 9648 105 105 9633 9782	
41 33 6C -3C 35 35 52 46 41 34 9C 0 1C8 1C8 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 3O 28 28 3C 22 42 37 6C 15 19 19 21 29 C 43 38 6C -3O 26 26 34 36	193 193 8315 8465 875 875 924C 9397 99 99 9396 9545 81 81 95C7 9648 105 105 9633 9782	
41 34 9C 0 108 108 5C 57 41 35 6C 15 18 18 57 49 41 36 3C 30 28 28 3C 22 42 37 6C 15 19 19 21 29 643 38 6C -30 26 26 34 36	875 875 924C 9397 99 99 9396 9545 81 81 95C7 9648 105 105 9633 9782	
41 35 6C 15 18 18 57 49 41 36 3C 3O 28 28 3C 22 42 37 6C 15 19 19 21 29 743 38 6C -3O 26 26 34 36	99 99 9396 9545 81 81 9507 9648 105 105 9633 9782	
41 36 3C 30 28 28 3C 22 42 37 6C 15 19 19 21 29 743 38 6C +30 26 26 34 36	81 81 9507 9648 105 105 9633 9782	
42 37 6C 15 19 19 21 29 C 43 38 6C -30 26 26 34 36	105 105 9633 9782	
~43 38 6C -30 26 26 34 36		
	0.40 0.40 00.40 00.48	
	143 143 9810 9961	
48 39 6C -15 33 33 36 35	182 182 10028 10178	
- 53 40 3C -15 29 29 30 21	84 84 1C142 1C283	
-54 41 30 45 7 7 14 14	20 20 10176 10317	
56 42 30 45 13 13 14 14	38 38 10228 10369	
57 43 9C C 89 89 32 48	720 720 10980 11137	
_57 44 3C 0 5 5 49 33		
58 45 90 -15 122 122 30 47	988 988 12062 12220	
58 46 30 -30 7 7 49 33	20 20 12131 12273	
59 47 60 15 31 31 21 28	171 171 12323 12472	
-68 48 3C C 4 4 29 21	12 12 12364 12505	
70 49 60 15 22 22 22 29		
71 5C 12C 0 35 35 64 81	375 375 12946 13111	
- 73 51 9C 15 65 65 91 83		
80 53 90 0 37 37 67 67		
81 54 3C C 14 14 5C 35	41 41 14220 14362	
86 55 60 +30 20 20 22 31	310 11C 14352 14503	
e7 56 6C -30 26 26 38 38	143 143 14533 14684	
87 57 120 0 66 68 67 61	728 728 15328 15493	
T88 58 90 0 25 25 90 82	203 203 15621 15778	
99 59 60 15 LC 1C 57 48	55 55 (5733 15881	
89 60 30 30 26 26 29 22	75 75 15837 15978	
_ 89 61 9C 0 26 26 33 50	211 211 16081 16239	
90 62 60 -15 12 12 58 50	66 66 16205 16355	
96 63 60 -30 8 8 37 37	44 44 16286 16436	
97 64 60 30 16 16 37 35	88 88 16411 16559	
103 65 90 0 86 86 45 54	697 697 17153 17310	
104 66 60 -15 38 38 52 45	209 209 17414 17564	
104 67 90 15 28 28 43 49		
-105 68 6C C 41 41 52 45	226 226 17962 18111	×
105 69 120 0 35 35 62 78	375 375 18399 18564	
166 76 36 -30 65 65 71 48		
-106 71 6C 3C 34 34 21 28	187 187 18867 19016	

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.13	7.2	3 C	3 C	3	Э	29	Approv 21	23		18919	1.9060	BIF-00	7/D-008	1-74
117	73	60	-15	45	45	20	28	248		19187		-	Annual of the State of the Stat	
118	74	3.0	0	7	7	28	20	20		19235		1:	arca 35, 835	60 KM 4
.19	75	3 C	-30	2 C	20	13	14	58	5.8	19306		144	1 112	400 Em 6
119	76	30	15	25	25	14	13	73	73	19393		THE	M	-
120	77	6 C	-15	31	31	20	29	171	171		19734			
.21	78	60	15	3.8	38	34	33	209		19827				
_2%	79	30	45	22	22	28	20	64		19919				
122	2.3	90	О	37	37	33	5 C	300	300	20252	20410			
₹.23	81	3.0	-3C	6	6	48	32	17		20317				
.23	82	9 C	0	35	35	3 T	46	284		20632				
123	83	3 C	-15	31	33	47	35	90		20769				
129	84	3.C	C	6	6	15	14	17		20801				
. 34	85	3 C	-45	4	4	14	15	12		20827				
£35	86	30	45	31	31	14	13	90	9°C	20931				
137	87		-15	1 C	10	13	14	29		20973				
.37	88		-30	13	1.3	21	30	72		21066				
37	89	6 C	0	17	17	37	36	94		21197				
137	9 C	90	0	3.9	35	5 C	58	316		21563				
-4.38	91	60	15	12	12	56	47	66		21685			4	
139	92	30	0	13	13	2.8	20	38		21751				
139	93		-15	. 7	7	21	3 C	39		21811				
144	94	30	-15	14	14	30	22	41		21862		,		
.52 .53	95 96	6 C	30 -45	1.9 6	19	21 28	28 21	105		22C88 22C53			*	
153	97	90	0	49	6 49	32	47	397		22482				
153	98	60	-30	30	3 C	54	48	165	165					
154	99	6.0	15	37	37	38	36	204		22943				
155	100	3.0	30	11	11	28	21	32		23003				1
755	101	6.0	-15	56	56	20	28	308	309	23331				
	102	9°C	15	19	19	49	56	154	154	23534				
160	103	6 C	3 C	10	10	57	48	56		23647				
165	3.04	3 C	C	la	4	28	22	12		23687				
167	105	3 C	15	15	15	14	13	44		23745	23886			
368	4.06	6 C	3.0	15	19	21	28	105		23871	24019		τ.	
169		9 C	C	44	44	47	5.6	356		24274	24431			
176		3 C	30	3.4	34	49	33	97	97		24561			
171	109	3 C	-3C	Ġ	ò	14	3.5	26		24460				
171	110	60	-15	5.1	21	21	29	116		24597				
171		6 C	1.5	16	le	37	36	88		24722				
	112	6 C	30	16	16	38	3.8	83		24848		4		
	113	60	15	19	19	36	36	105		24989				
176		60	Ç	15	15	37	37	83		25109				
	115	9.0	0	35	35	49	57	284	284					
185		60 40	3.0	19	19	57	45	105		25604				
_186 _186	117	6C	-15 30	12 52	12 52	36 36	38	66 504		257C6 26C28				
199	119	6 C	0	7	7	3.6	34 37	286 39	39	26103				
200	120	30	45	8	8	29	20	23		26155				
	121	120	ć	34	34	50	74	364	364	26569				
24 M N	est star de	- St. 54	w		-	A 14		Jan Mary	- Fr. 154 114	Section of the F	www.r.wente			

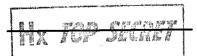
C05	12	774	8	. x			Approv	ed for Re	lease: 2	025/07/25	C05127748
201	122	3 C	C	10	10	74	51	29	29	26672	26814
202	123	6 C	0	46	46	21	29	253	253	26946	27095
-2.03	124	30	30	31	31	29	21	90	90	27065	27206
:16	125	3 C	30	14	14	14	14	41	41	27120	27261
216	126	120	0	3 c	36	51	75	385	385	27556	27721
216	127	60	15	19	19	82	65	105	205	27743	27891
218	128	3 C	15	4	4	29	22	12	12	27784	27925
218	129	6 C	C	22	22	22	30	121	121	27927	28076
225	13C	3 C	30	7	7	29	21	2.3	2 C	27976	28117
225	131	6 C	· C	4	2	21	3 C	22	15	28C19	28162

BIF-007/D-0081-74

1. 1208-2

B.	CAMERA	CPERATICAS	SUMMARY	REV	225,	CP	131	THPCUGH- REV	674 +	ОÞ	364.

REV	MSA CP	SCA	SCC	FRAI	ES	INTE	RCP	PHCT	C-FT	CUM-TU	-FEET
nettes	NUM			FWC	AFT		AFT	FWD	AFT	FWD	AFT
225	131	6 C	0	7	ç	0	Ö	43	51	43	51
236	132	3.0	-30	4	4	85	81	12	12	144	144
_232	133	6 C	15	3.1	31	22	29	171	171	337	344
232		90	· Ĉ	5.9	59	49					
	134			4		2.2	57	478	478	864	879
239	135	3 0	-15	.6	6	49	33	17	17	930	929
_236	136	-60	C	8	8	SC	29	44	44	994	1002
2.3 6	137	3 C	3 C	-8	8	29	20	23	23	1046	1045
247	138	120	C	26	26	38	62	278	278	1362	1385
248	139	6 C	15	16	16	65	53	8.8	3.8	1519	1526
24.6	140	3 C	-3.C	26	26	28	21	75	75	1622	1622
248	141	9 C	-15	54	54	3.5	51	437	437	2094	2110
249	142	-9 C	C	19	15	69	68	154	154	2317	2332
-250	143	60	15	31	31	54	46	171	171	2542	2549
250	144	9 C	С	10	1.C	47	55	81	81	267C	2685
25%	145	60	15	16	1.6	54	46	88	8.8	2812	2819
251	146	60	15	44	44	37	37	242	242	3091	3098
252	147	60	-15	8	8	34	35	44	44	3169	3177
252	148	3 C	-15	16	16	27	19	46	46	2342	3242
253	149	30	15	10	1 C	14	13	29	29	3285	3284
~253	150	60	-15	23	23	20	29	127	127	3432	3440
258	151	3 Č	-15	6	6	30	22	17	17	3479	3479
598	152	30	-30	23	23	14	13	67	67	3560	3559
-268	153	3 C	-3C	14	14	14	15	41	41	3615	3615
269	154	6 C	15	16	16	20	27	8.8	88	3723	3730
273	255	6 C	15	16	16	35	35	8.8	88	3846	3853
281	156	90	15	9.8	9.8	48	56	754	754	4688	4703
288	157	9.0	- 10 0	19	19	6.2	63	154	154	1904	4926
284	158	60	Ċ	3.9	15	5 C	42	105	105	5 C 5 S	5067
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313	165	3.0	4.5	2.8	3.5	48	31	18	13	6743	6742
_313	166	50	-15	42	42	32	5 C.	340	340	7125	7132
314	167	120	C	29	29	85	91	310	31 C	7510	7533
329	168	60	С	31	31	8.1	€5	171	171	7762	7769
329	169	3.0	30	Li	11	29	21	32	32	7823	7822
-329	170	3.0	-30	24	24	14	14	70	70	7907	7906
330	2.72	6 C	15	43	43	22	3 C	237	237	8166	8173
331	172	60	-3C	3	8	37	37	44	44	8247	8254
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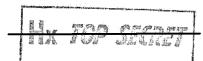
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526	282	6 C	C	19	19	22	3 C	105	105		18488
- 27	283	3.0	45	4	4	29	21	12	12	15513	18521
127	284	3.0	-3C	1 C	10	14	15	30	3.0	19557	18566
527	285	3 C	-15	14	14	14	14	41	42	19612	13621
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52.8	287	90	C	35	35	34	50	284	284	19964	18988
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542	295	3 C	-15	14	14	14	14	41	41	20616	19623
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543	297	9 C	C	35	35	29	44	284	284		19984
544	258	3 C	-45	3.2	32	44	25	93	93	21099	20106
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548	302	6.0	-30	13	13	21	49	72	72		20419
556	3C3	3 C	-15	i.C	1.0	29	21	29	29		20469
559	304	6.C	15.	25	25	19	26	138	138		20633
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559	307	3 C	1,5	Z.	4	13	1.3	12	1.2		20716
560	308	3 C	0	13	13	14	1.2	38	3.8		20757
561	309	3.0	-45	2 c	26	13	14	7.5	7.5	21849	20856
361	31 C	30	15	16	16	14	13	46	4.5		20915
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572	312	3 C	-30	35	35	29	22	102	102		21146
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575	325	6.0	15	34	34	56	47	187	187		21859
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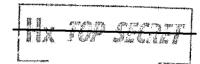
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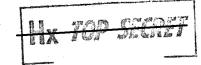
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Approved for Release: 2025/07/25 C05127748

В. CAMERA OPERATIONS SUMMARY REV 674 CP 364 THROUGH REV 1111 OP 577

CP	3EV	MSN CP	SCA	scc	FRAN	ES		ERCP	PHOT	C-FT	CUM-TU	-FEET
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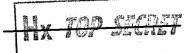
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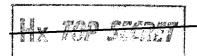
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	1 /	/ ユ	O,				Approv	ed for Re	elease: 2	025/07/25	C05127748	BIE-0	07/0900	81-74
: 15C	557	6 C	-15	45	45	37	37	248	248	22713	2 781	W. F I		
2090	558	30	3 C	13	13	29	2.0	38	3.8	2278C	21839	Г		
1092	559	90	0	62	62	34	5 C	502	502	23316	22391		变 你 們	En Las Ca
(7.93	56C	3 C	3 C	7	7	48	32	20	20	23384	22443	HX	101	ed in the
)93	561	3 C	15	7	7	13	13	20	20		22476	H 6.74	AN NOW BY	ecor sear real E
1094		60	15	52	52	20	28	286	286	23723	22790	L		
-294		6 C	15	3,9	19	36	36	105	105		22931			
199	564	3 C	C	5	5	28	2.0	15	15		22966			
1106	565	30	O	22	22	13	13	64	64	23984	23043			
11C6	566	3 C	3 Ç	14	14	13	13	41	41		23097			
1.06		3 C	-30	-8	-8	15	16	23	23	24076	23136			
30.4	568	90	0	37	37	34	49	300	30 c	2441C				
1109		60	Č	34	34	56	48	187	167	24653	23720			
1,09	570	3.0	-15	10	10	-28	21	29	29	2471C				
1109	571	3 C	15	8	8	14	14	23	23	and the state of t	23807			
1169	572	30	Ĉ	16	16	14	14	46	46	24807	23867			
3-1.09	573	3 C	-3C	7	7	14	14		20	24641	23901			
			4	11	11	14		20	32	24887	23947			
0.09	574	3.0	-45				14	32						
1110	575	3 C	3 C	19	19	14	13	55	5.5	_	24015			
1110	576	6 C	3.0	9	9	22	29	5 C	5 C					
1.11	577	3 C	-15	65	65	29	23	187	188	25244	24305			



CAMERA EPERATIONS SUMMARY REV 1111 OP 577 THROUGH REV 1694 OP 774

ĸEV	MSN CP	SCA	scc	FRAN	'ES	INTE	ERGP	PHOT	C-FT	CUM-TU	-FEET
Prome .	NUM			FNC	AFT	FWC	AFT	FHC	FFT	FWD	AFT
n. 19 4	577	3 C	-15	13	13	0	C	36	35		
1122	578	3.0	-30	14	14	77	77	41	41	36 154	35 153
7.22		3 C	3 G		24	14		70			236
	579			24	,,		13		7 C	238	
1 23	580	30	-30	24	14	14	15	41	41	293	292
1123	581	3.0	30	11	11	14	13	32	32	335	337
1125	582	3 C	3.0	20	20	14	14	29	29	382	380
25	583	3 C	30	7	7	14	14	20	20	416	414
1126	584	60	15	28	28	21	29	154	154	591	597
1.26	585	6.C	-15	13	13	35	36	72	72	698	705
3.30	586	3.0	0	5	5	29	20	15	15	742	740
239	587	9 C	C	43	43	33	49	348	348	1123	1137
1141	588	90	0	34	34	67	67	275	275	1465	1479
7.41	589	30	-3C	21	21	48	33	61	61		1573
42	59C	3 C	-3C	10	10	14	14	29	29	1617	1616
1142	551	3 C	-15	11	11	14	3.4	32	32	1663	1662
1142	592	3 C	-3C	9	9	14	13	26	2€	27C3	1701
1,42	553	3 C	-30	12	12	13	14	35	35	1,751	1750
2142	554	3 C	C	7	7	14	13	20	2.0	1785	1783
1148	595	5 C	-15	22	22	2.0	28	121	121	1926	1932
1.48	596	3 C	-15	8	8	29	21	2.3	23	1978	1976
_155	597	6 C	3 C	7	7	21	28	39	39	2038	2043
1155	598	60	0	16	16	36	36	8.8	8.8	2162	2167
₹ 57	599	.3 C	-15	13	1.3	28	21	38	36	2228	2226
1.57	ECC	3 €	-3C	12	12	14	14	35	35	2277	2275
1158	601	6.C	15	26	26	21	28	143	143	2441	2446
1158	602	60	C	13	13	36	37	72	72	2549	2555
158	603	20	3 C	Lį.	L	28	19	1.2	12	2589	2586
4,159	6C4	60	15	5 C	50	2 %	29	275	275	2685	2890
1164	€ C 5	6 C	-15) C	C	33	34	55	55	2973	2979
167	606	60	15	19	1.5	31	3.0	1,05	105	3109	3114
169	697	3.0	0	1.0	10	25	13	29	29	3163	3161
1165	833	3 C	15	11	11	13	12	32	32	3208	3205
-169	€09	3 C	-3¢	5	5	13	24	15	1.5	3236	3234
171	ELC	60	-15	10	10	20	28	55	55	3311	3317
1171	611	6 C	-15	24	34	3.5	35	187	187	3533	3539
1171	612	é C	15	7	7	37	36	39	35	3609	3614
172	613	6 C	15	É	6	36	36	3.3	33	3678	3683
4174	614	60	-15	4	4	35	36	22	22	3735	3741
1174	615	3.0	C	19	19	27	18	55	55	3817	3814
174	816	6.0	-15	14	14	20	30	77	77	3914	3921
174	617	3 (C	8	e	25	20	23	23	3966	3964
1180	618	30	-30	26	26	13	13	75	75	4054	4052
-183	615	3 C	-30	11	11	14	14	32	3.2	41CC	4098



C03127	740				Approve	ed for Rel	ease: 20	025/07/25	05127748
2 81 620	30 15	5	5	14	23	1.5	15	4129	4126
1183 621	30 30	22	22	13	13	64	64	4206	4203
1-87 622	60 30	19	19	19	27	1.05	105	433C	4335
: .87 €23	6C 15	2.5	25	35	35	138	138	4503	45C8
1187 624	60 0	10	1.0	36	36	55	55	4594	4599
1189 625	6C 0	16	16	35	35	88	88	4717	4722
1.9C 626	60 -15	27	27	34	35	149	145	490C	4906
1.90 627	60 30	13	13	35	34	72	72	5007	5012
1190 628	6C -15	4	4	36	37	22	22	5065	5071
Tigi 629	90 - 0		74	47	54	599	599	5711	5724
: 203 630	6C 15		ìC	54	46	55	55	5820	5825
1207 631	6C 0		7	36	37	39	39	5895	5901
218 632	3C C	5	5	29	21	15	15	5939	5937
220 633	6C -15		19	20	27	105	1 C 5	6064	6069
1221 634	6C -15		îí	32	33	61	61	6157	6163
1221 635	60 0	7	7	33	32	39	39	6229	
223 636	60 30		19	3.5	34	1 C 5	105	6369	6373
236 637	9.0 0		10	46	55	81	81	6496	65CS
1236 638	6C 15		25	54	46	138	138	6688	6693
37 639	60 15		16	36	36		98	6812	6817
245 640	60 15		10	36	36	55	55	6903	6908
1300 641	60 0	6	6	79	39	33	33	7C15	6980
-30C 642	6C 15		q	35	Č	105	C	7155	6980
302 643	3C -45	29	29	29	20	84	84	7268	7084
1302 644	90 15	22	22	34	49	178	178	7480	7311
1303 645	60 30	13	13	55	46	72	72	7607	7429
303 646	6C -15		10	35	36	55	55	7657	7520
.303 647	60 15	22	22	36	36	121	121	7854	7677
1304 648	90 0		37	48	56	300	300	8202	8633
304 649	30 0		īi	48	33	49	49	8299	
305 65C	60 -15	35	35	21	29	193	193	8513	8337
1309 651	3.0 0	- 8	.8	29	21	23	23	8565	638 1
4316 652	60 30		13	20	26	72	72	8657	8479
316 653	60 -15	22	22	33	35	121	121	8611	8635
1317 654	60 15	9	9	37	36	50	5 C	8898	8721
1318 655	30 -30	ıć	& Ć	28	21	29	29	8955	8771
218 656	60 -15		17	22	3 C	94	54	9071	8895
_319 £57	60 -15		26	3.6	3.6	143	143	9250	9674
1320 658	6C -15		74	36	36	407	467	9653	9517
7320 639	30 -30	9	9	29	21	26	26	9748	9564
320 659 321 66C	6C 15	13	13	21	28	72	72	9841	9664
1321 601	60 -30		14	36		77	77	9954	9778
4325,662	90 0		16	48	5.5	130	130	10132	9963
327 663	30 30	8	8	48	31	23	23	10203	10017
1332 664	90 0	22	2.2	32	48	178	178	10413	10243
1333 665	6C -15	21	21	55	48	116	116	10584	10407
334 666	6C 15		17	36	35	94	94	10714	10536
.324 667	60 -30	5	5	37	38	28	2 d	16779	10502
1335 668	60 15	21	21	36	35	116	116	10931	10753
336 665	6C 15		122	35	35	671	671	11637	11459
		***		-	-	7.2	₩ , 1 ×	in with many at	**************************************





C05	512	774	18				Appro	ved for R	elease:	2025/07/25	C0512774	⁴⁸ BIF-00	7/0000	1 - 74
1 136	670	3 C	15	5	5	29	20	15		11681		DIF-00	110-000	1-74
1348			-15	14	14	20	29	77		11778		T	21	a Min. Stock
1349		60	-15	13	13	37	37	72	72	11887		Mar	TOD	6 F./
1149		60	С	25	25	37	37	138		12062	11884	- 111/1	R SFD	BOD SHIP Y
1.250	674	6 C	-15	29	25	36	37	160		12258	12081			
1351	675	60	15	16	16	37	36	88		12383	12205			
7364	676	3 C	-30	49	49	28	21	142		12553	12368			
1 165		50	С	31	31	34	49	251		12838	12668			
1366		9 C	0	73	73	67	67	591	591	13496	13326			
1-166		S C	0	11	11	68	68	89	89	13653	13483			
167	680	3 C	3.0	45	45	48	32	131	131	13832	23646			
1368		60	15	2.5	25	22	29	138	381	13952	13813			
1365		6 C	15	8.5	£ \$-	36	37	490	49¢	14518	14340			
374		3 C	3 C	17	1.7	29	21	43		14596				
1375		5 C	G.	38	38	21	29	209		14826				
1382	6.85	SC	O	22	22	48	56	178		15052				
382		6 C	15	21	21	57	49	116		15225				
383			-15	14	14	36	37	77		15338				
1383			-15	13	13	37	37	72		15447				
184	669	6 C	1.5	3.0	3 G	37	36	165		15649				
185		90	0	87	87	48	56	705		16402				
1397		60	-15	14	14	56	4.8	77		16535				
1397		60	20	15	15	37	37	83	2.3					
255 2400			-30 -15	13	13	29 22	2.2 3.0	38 83	3.8	16722				
	695			15	15	3.8		72						
1401	696	3.0	-15 30	13 33	13 33	29	37 21	96		16937 17062				
	697	3·0	15	<i>33</i>	9.9 9	15	15	26		17103				
101 1402	698	60	15	17	17	ĒŠ	30	94			17C41			
1413	6.9.9	9.0	10	38	3.6	45	54	308		17573	17403			
415	70°C	60	15	26	26	50	42	143		17766				
1416	701		-15	9	9	33	34	5 C		17849	17672			
1417	702	90	Ĉ	34	34	44	51	275		18168				
122	703		-30	9	ç	45	30	2.6		18239				
×429	704	90	G	54	54	31	40	437			18537			
1430	765	9.0	Ö.	5.0	E C	6.6	6.6	405	405		19008			
737	766	6.C	25	3.0	3·C	54	46	165		19397	19219			
431	707	3.C	O:	5	5	27	19	15		19439	19253			
1433	708	6 C	Ç	S	S.	20	31	50	5 C	19509	19334			
445	709	90	C	34	34	45	5.2	275	275	18828	19661			
449	710	6C	-15	13	13	53	45	7.2	72	19954	19778			
1449	711	é C	3.0	S	9.	35	34	50		20039				
1462	712	6 C	Û	13	T 3	36	3 e	72		20147				
456	713	6.C	15	17	17	34	34	94		20275				
466	714	6 C	О	5	S	35	3.5	50			20183			
1471	715	9.0	C	16	16	48	56	130		20538				
481	716		-15	25	25	57	49	138		20733				
4.22	717	45	1.5	1 3	7.2	24	36	7.2	7.2	20841	20864			

6 C

3.0

3 C

482 717

1482 718

487 719

15

30

15

13

9

10

13

9

i C

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28

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36

2.0

14

72

26

29

TOO CECONE

72 20841 20664

26 20895 20710

29 20938 20753

BIF-007/D-0081-74

IX TOP SECRET

						Applo	ved for ite	sicase. 2	2020/01/20	00012//-
720			14	14	22	31	77	77	21037	20861
721	3 C	-3C	13	13	29	21	38	3.8	21104	20920
7.22	30	-30	12	12	14	14	35	35	21153	20969
723	6 C	C	13		21					
										21201
										21427
										21521
										21868
732		C	6	6	14	14	18	1.8	22C84	21900
733	3 C	C	8	8	14	14	2.3	23	22121	21937
	60	-15	47	47	21			259		22225
										223C1
										22730
		-10								22882
										22923
										23002
									23326	23159
				46						23312
744	3 C	3 C	19	19	13	13	55	55	23555	23380
745	3 C	Ö	6	6	13	13	1.7	17	23585	2341C
746	3.0	3.0	23	2.3	14	14		6.7	23666	23491
					14					23592
										23672
										237C2
										24715
										24782
										24877
									ZDZTU	25112
										25162
										25152
										25221
					17		83	8.8		25334
	30	30	1.3	13	29	20	38	38	25567	25392
7.61	30	1,5	8	8	14	15	23	23	25604	25430
762	6 C	-15	14	14	22	3 C	77	77	25703	25537
			7							25578
			5							
754										
102	200	-15	よう	7,2	14	24	22	ככ	ZOICC	20020
	721 72234567 72234567 72237 7331 7333 73367 7343 7344 7443 7443	721 722 722 722 722 722 722 723 723 723 723	721 30 -30 c	721 3C -3C 13 722 3C -3C 13 723 6C -C 15 724 3C -15 725 3C -15 726 6C 15 727 3C -3C 15 728 3C -15 729 6C -15 721 3C -C 21 722 3C -C 15 723 3C -C 15 724 3C -C 15 725 3C -C 15 727 3C -C 21 728 3C -C 15 728 3C -C 15 728 3C -C 15 728 3C -C 15 738 3C -C 15 748 3C -C 15 758 3C -C 15	721 3C -3C 13 13 722 3C -3C 13 13 724 3C -15 5 25 726 6C 15 36 36 727 3C -3C 15 11 728 3C -3C 15 12 729 6C -15 12 729 6C -15 15 15 720 6C -15 15 16 721 3C -3C 15 17 722 3C -3C 15 17 723 3C -15 17 724 3C -15 17 725 3C -15 17 726 6C -15 17 727 3C -3C 15 17 728 3C -15 17 729 6C -15 17 721 3C -2C 22 721 3C -2C 22 722 3C -15 17 723 3C -15 17 724 6C -2C 22 724 3C -2C 22 724 3C -2C 22 724 3C 3C 3C 3C 3C 725 3C -15 18 727 728 3C -15 18 728	721 3C -3C 13 13 29 722 3C -3C 13 13 21 723 6C -C 13 13 21 724 3C -15 25 25 13 726 6C 15 36 36 21 727 3C -3C 3C 25 25 28 728 3C -3C 15 16 26 36 727 3C -3C 15 16 22 728 3C -3C 15 16 21 729 6C 15 16 21 11 12 729 6C 15 16 47 47 21 729 6C 15 17 17 29 730 6C -15 17 19 19 20 731 3C -16 19 19 20 732 3C -16 19 19 20 733 3C -15 19 19 20 734 6C -15 19 19 20 735 3C -15 19 19 19 737 6C 3C -3C 77 741 6C -C 0 22 22 26 742 3C -3C 76 3C	72C 6C -15 14 14 22 31 721 3C -3C 13 13 23 28 722 3C -3C 13 13 21 28 723 6C -15 25 26 21 28 724 3C -15 36 25 26 21 28 725 3C 15 36 25 26 21 3 12 728 3C -3C 15 36 25 28 21 728 3C -3C 15 36 25 28 21 728 3C -3C 15 36 25 28 21 728 3C -3C 15 28 25 28 21 728 3C -15 1C 1C 22 36 727 3C -8 8 8 14 14 729 6C 15 15 16 14 14 729 730 6C -15 15 16 14 14 733 3C -15 15 19 20 57 731 3C -15 19 19 20 57 732 3C -15 19 19 20 57 733 9C -15 19 19 20 20 736 3C -15 19 19 20 20 736 3C -15 19 19 20 20 737 74C 3C -3C -3C -3C -3C -3C -3C -3C -3C -3C	72C 6C -15 14 14 22 31 77 721 3C -3C 13 13 29 21 38 723 6C C 13 13 21 28 72 724 3C -15 9 9 28 21 73 725 3C 15 25 25 13 12 72 726 6C 15 36 36 21 28 198 727 3C -3C 25 25 13 12 73 728 3C -3C 25 25 28 21 73 728 3C -3C 25 28 21 73 73 729 6C -15 10 10 22 29 55 730 6C -15 47 47 21 29 259 735 3C 3C 45 54 14 14 18 18 19 20 27 <td>72C 6C -15 14 14 22 31 77 77 721 3C -3C 13 13 29 21 38 38 722 3C -3O 12 12 14 14 35 35 723 6C C 13 13 21 28 72 72 724 3C -15 25 25 13 12 73 73 726 3C 15 25 25 13 12 73 73 726 3C -3C 25 25 28 21 73 73 728 3C -3C 25 25 28 21 32 39 729 3C -3C 16 12 22 29 55 15 15</td> <td>72C 6C -15 14 14 22 31 77 77 21037 721 3C -30 13 13 29 21 38 38 211C4 722 3C -30 12 12 14 14 35 35 21153 723 3C C C 13 13 21 28 72 72 21246 724 3O -15 5 9 28 21 26 26 21300 725 3C 15 25 25 13 12 73 73 21386 726 6C 15 3C 36 21 28 21 73 73 21766 728 3C -30 11 11 13 14 32 22 21751 729 3C 20 24 44 42 22 25 55 55 <</td>	72C 6C -15 14 14 22 31 77 77 721 3C -3C 13 13 29 21 38 38 722 3C -3O 12 12 14 14 35 35 723 6C C 13 13 21 28 72 72 724 3C -15 25 25 13 12 73 73 726 3C 15 25 25 13 12 73 73 726 3C -3C 25 25 28 21 73 73 728 3C -3C 25 25 28 21 32 39 729 3C -3C 16 12 22 29 55 15 15	72C 6C -15 14 14 22 31 77 77 21037 721 3C -30 13 13 29 21 38 38 211C4 722 3C -30 12 12 14 14 35 35 21153 723 3C C C 13 13 21 28 72 72 21246 724 3O -15 5 9 28 21 26 26 21300 725 3C 15 25 25 13 12 73 73 21386 726 6C 15 3C 36 21 28 21 73 73 21766 728 3C -30 11 11 13 14 32 22 21751 729 3C 20 24 44 42 22 25 55 55 <

C05.	12/	/4	8				Approve	ed for Rel	ease: 20	25/07/25	05127748	BIF-0	07/D-00	81-74
591	77C	3 C	-3C	10						26143			0.,0 00	, , , , , , , , , , , , , , , , , , ,
1693	771	6 C	C	7	7	22	29	39	35	26204	26137		,	
1693	772	3 C	-30	9	9	28	21	26	26	26258	26184	Llu	TAB	SECRET
593		90	C	15	15	36	51	122	122	26416	26357	TIA		الأسامة أنسان مناشيه
_394	774	6 C	-15	34	31	57	49	185	167	26658	26573	1		etermoise
						32	62			26690	26635	September		***************************************